

Gelatine cavity dynamics of high-speed sphere impact

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We investigate the impact and penetration of a solid sphere passing through gelatine at various impact speeds up to 143.2 m s^{-1} . Tests were performed with several concentrations of gelatine. Impacts for low elastic Froude number Fr_e , a ratio between inertia and gelatine elasticity, resulted in rebound. Higher Fr_e values resulted in penetration, forming cavities with prominent surface textures. The overall shape of the cavities resembles those observed in water-entry experiments, yet they appear in a different order with respect to increasing inertia: rebound, quasi-seal, deep-seal, shallow-seal and surface-seal. Remarkably, similar to the $We-Bo$ phase diagram in water-entry experiments, the elastic Froude number Fr_e and elastic Grashof number Gr_e (a ratio between gravity and gelatine elasticity) classify all five different phenomena into distinguishable regimes. We find that Fr_e can be a good indicator to describe the cavity length H , particularly in the shallow-seal regime. Finally, the evolution of cavity shape, pinch-off depth, and lower cavity radius are investigated for different Fr_e values.

Key words: breakup/coalescence, multiphase flow

1. Introduction

Gelatine has received considerable attention in the scientific community as it is an effective analogue for human tissue. For example, gelatine is used for studies on traumatic brain injury (Kang *et al.* 2017, 2018; Pan *et al.* 2017) and fabrication of drug delivery systems (Tagawa *et al.* 2013; Battula, Menezes & Hosseini 2016; Moradiafrapoli & Marston 2017; Kiyama *et al.* 2019). However, because the properties (e.g. shear modulus G) are rate-sensitive, the deformation dynamics is challenging to model.

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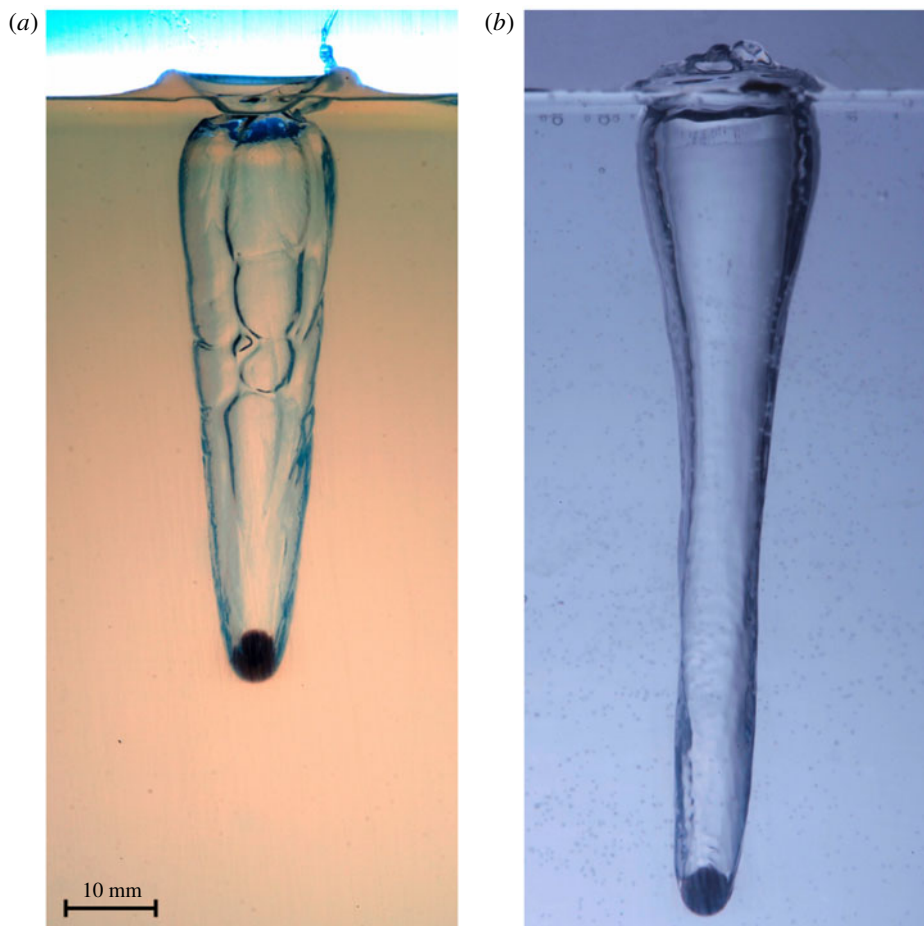


FIGURE 1. (Colour online) Solid spheres introduce different cavity dynamics between gelatine and water with the same Froude number $Fr = u_0^2/(gR) \sim 1.0 \times 10^5$, where the impact speed is $u_0 \sim 15 \text{ m s}^{-1}$, the gravitational acceleration is $g = 9.81 \text{ m s}^{-2}$ and the sphere radius is $R = 2.25 \text{ mm}$. (a) A copper-coated steel sphere impacts onto a 1 wt% gelatine surface and forms a conical cavity with distinct wavy surface textures. (b) In water, similar impact conditions produce a long and smooth cavity.

A current area of research is the penetration of a solid sphere into gelatine. When a sphere falls onto gelatine, two typical events occur depending on the impact velocity. For relatively small impact velocities, the sphere does not penetrate into the gelatine (Swain *et al.* 2014); instead, it bounces off. For higher impact velocities, a cylindrical cavity forms (Liu *et al.* 2012; Ryckman, Powell & Lew 2012; Wen *et al.* 2013; Swain *et al.* 2014; Veyssset *et al.* 2018). Here we find that while the cavities formed by spheres penetrating gelatine and water have some differences, they share many similarities as well. For instance, cavity shapes produced in gelatine and water (see figure 1) appear similarly shaped with both sealing near the free surface. In contrast, gelatine produces cavities having remarkably non-uniform cavity textures (see also Wen *et al.* 2013).

The classification of specific ‘cavity types’ can provide important information for understanding complex cavity dynamics. Cavity types in water and viscoelastic fluids have been studied by Akers & Belmonte (2006) and Aristoff & Bush (2009), respectively. In water, Aristoff & Bush (2009) classified cavities by the position of the cavity sealing event. By considering the effects of inertia, gravity and surface tension, they proposed a phase diagram of four cavity types using the Weber number We and the Bond number Bo . More recently, Speirs *et al.* (2019) revealed that the boundaries for each cavity type in the We – Bo mapping shift with changes in the sphere–water wetting angle and surface roughness. In viscoelastic fluids, Akers & Belmonte (2006) reported a unique surface texture on the cavity walls (in a solution of 80 mM CPCl and 60 mM NaSal) where a phase diagram was proposed considering both sphere inertia and liquid elasticity. Although several different cavity types in gelatine have been reported (Liu *et al.* 2012; Wen *et al.* 2013; Liu, Fan & Li 2014*a*; Liu *et al.* 2014*b*; Veysset *et al.* 2018), mapping the cavity regimes remains an open question.

Here, we examine high-speed images of the gelatine deformation in the wake of a solid sphere impact. By varying the impact speed u_0 ($0.4 \text{ m s}^{-1} \leq u_0 \leq 143.2 \text{ m s}^{-1}$) and gelatine concentration C ($1 \text{ wt}\% \leq C \leq 10 \text{ wt}\%$), we show the formation of four different types of cavities similar to those observed in water. Based on our parametric study, we classify the cavity types based on their sealing position and discuss their length and dynamics. We then propose a phase diagram using two relevant non-dimensional numbers.

2. Experimental set-up

A schematic of the experimental set-up is shown in figure 2(*a*). We fill an acrylic container ($100 \text{ mm} \times 100 \text{ mm} \times 250 \text{ mm}$) partially with water or gelatine to a height of 150 mm. A copper-coated sphere (radius $R = 2.25 \text{ mm}$, density $\rho_s \sim 6800 \text{ kg m}^{-3}$) is shot from an air rifle (Crossman 760) into the pool. A spray coating (Glaco mirror coat zero) was used to make the sphere hydrophobic and provide a single contact angle (141° , Speirs *et al.* 2019). The sphere travels through the air and impacts the pool surface with a speed of u_0 . A high-speed colour camera (Phantom v2510) is used to record the impact event and the cavity formation up to 50 000 f.p.s. with a 0.2 mm pix^{-1} spatial resolution. Matlab image analysis is used to capture the motion of the sphere and cavity. Measurements of the cavity dimensions at the time of pinch-off are defined by the free body diagram in figure 2(*b*).

The water–gelatine mixture ($1 \text{ wt}\% \leq C \leq 10 \text{ wt}\%$) is prepared by boiling distilled water (approximately 0.75 L) and mixing with gelatine powder (Nowfoods, Beef Gelatin Powder) for 12 min. The concentration of gelatine is controlled based on the weight percentage of gelatine used. The solution is kept in a refrigerator overnight (22 to 26 h) and then in the laboratory at room temperature ($\sim 23^\circ\text{C}$) for several hours before conducting the impact experiments. Although the bulk temperature of the gelatine and the humidity were not measured, we assume that they only cause small variations in the penetration event (Jussila 2004).

We present the rheological properties and density of all concentrations of gelatine in table 1. All rheological tests are performed using a TA Instruments AR 2000 rheometer where the temperature of the geometry is set at 4°C . The elastic (storage) modulus G' and the viscous (loss) modulus G'' are measured using strain-sweep tests where the shear modulus, also known as the complex modulus, is calculated as $G = \sqrt{G'^2 + G''^2}$. Here the gelatine stiffness increases with concentration C , and G' is much larger than G'' for all concentrations. The ratio of G' and G''

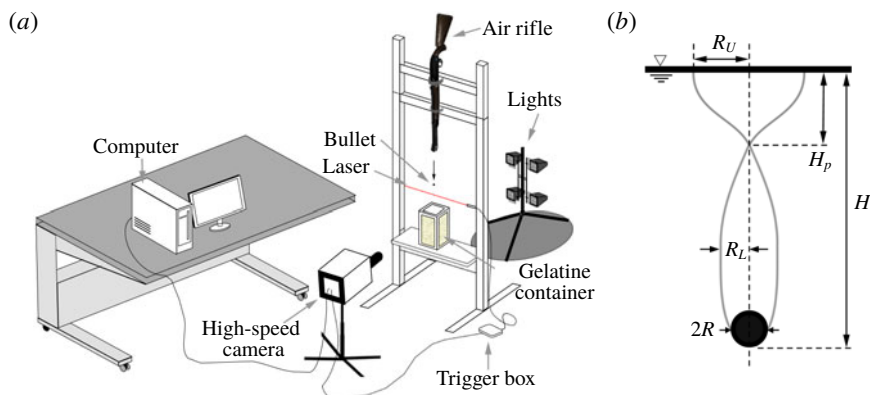


FIGURE 2. (Colour online) (a) Schematic of the experimental set-up. A copper-coated steel sphere is shot from the air rifle. A gelatine container is placed below the nozzle of the rifle. A high-speed camera films the cavity motion in the gelatine with diffuse back lighting. High-speed video is recorded and analysed on the computer. Photographs similar to figure 1 are taken with a Canon EOS 5D using a laser-sensor to trigger the camera. (b) Free body diagram. Here R is the radius of the sphere. Cavity dimensions are measured at the first pinch-off of the cavity: the total cavity length H , pinch-off depth H_p , maximum radius of the upper portion of the cavity R_U and the maximum radius of the lower portion of the cavity R_L .

values ($\tan \delta$) are presented in table 1 (see also supplementary material available at <https://doi.org/10.1017/jfm.2019.696>). The values are much smaller than unity, and the 1 wt% gelatine is slightly higher than the others, suggesting that the 1 wt% gelatine will flow relatively more easily when a large deformation is applied. Note that all the rheological properties are measured under a small strain regime (limitation of our rheometer) and thus these values may not perfectly reflect the features of gelatine dynamics under severe deformation (i.e. sphere impact).

The relevant non-dimensional parameters include the Froude number Fr , the Weber number We , the Bond number Bo , the elastic Froude number Fr_e and the elastic Grashof number Gr_e . Definitions and ranges of each parameter are listed in table 2, where ρ is the density of pool medium. The measured density of water is $\rho \sim 992 \text{ kg m}^{-3}$ (see supplementary material), the surface tension of water is $\sigma = 72 \text{ mN m}^{-1}$ and the gravitational acceleration is $g = 9.81 \text{ m s}^{-2}$. Note that we modified the definition of the elastic Froude number and the elastic Grashof number used in Akers & Belmonte (2006), where the density difference $\Delta\rho (= \rho_s - \rho)$ was adopted for both non-dimensional parameters. These numbers compare the shear modulus G with the inertia and gravity (buoyancy), while the Weber number and the Bond number compare the surface tension with inertia and gravity.

3. Observations

The most apparent difference between cavities formed in gelatine and water is the appearance of surface texture (figure 1). The surface texture varies depending on the gelatine concentration and sphere impact speed, where larger gelatine concentrations require higher impact speeds to produce the phenomenon (figure 3*c–f*). Figure 3(*c*) reveals that the surface texture stays at the formation location where the shape of the texture becomes more apparent with the radial expansion of the cavity. The images

C (wt%)	G' (Pa)	G'' (Pa)	$G = \sqrt{G'^2 + G''^2}$ (Pa)	$\tan \delta = G''/G'$	ρ (kg m ⁻³)
1	68	3	68	3.5×10^{-2}	1013
2	407	6	407	1.4×10^{-2}	1015
3	978	16	978	1.6×10^{-2}	1009
5	5 542	57	5 542	1.0×10^{-2}	1035
10	17 660	258	17 662	1.5×10^{-2}	1043

TABLE 1. Properties of the different gelatines. The elastic (storage) modulus G' , the viscous (loss) modulus G'' , the shear (complex) modulus G , density ρ and the gel fluidity represented by the angle $\tan \delta = G''/G'$ are presented for each gelatine concentration C . For comparison purposes, the typical stress caused by surface tension σ/R is approximately 32 Pa and the density of water was measured as 992 kg m⁻³. More details are provided in the supplementary material.

Parameter	Definition	Range
Froude number Fr	$u_0^2/(gR)$	$7.2 \times 10^0 < Fr < 9.3 \times 10^5$
Weber number We	$\rho R u_0^2/\sigma$	$3.8 \times 10^0 < We < 5.5 \times 10^5$
Bond number Bo	$\rho g R^2/\sigma$	6.8×10^{-1}
Elastic Froude number Fr_e	$\rho u_0^2/G$	$1.3 \times 10^0 < Fr_e < 7.7 \times 10^4$
Elastic Grashof number Gr_e	$\rho g R/G$	$1.3 \times 10^{-3} < Gr_e < 3.3 \times 10^{-1}$

TABLE 2. Definition and range of non-dimensional parameters.

do not reveal whether the surface texturing is plastic (permanent) or elastic; however, there is sufficient evidence that the cavity does appear to create a permanent hole in the gelatine pool (discussed later and in supplementary movie 3). While the exact cause of the surface texture is not known, we postulate it to be due to one or all of the following: crack propagation (Arakawa & Takahashi 1991), shear-induced cavity removal similar to viscoelastic fluids (Akers & Belmonte 2006) or surface-solid attachment similar to surface tension effects (Enriquez *et al.* 2012).

We find the cavity shape to be highly dependent on the gelatine concentration. The evolution of cavities in various media is first studied keeping the impact velocity constant ($u_0 \sim 30$ m s⁻¹). Similar to the events observed in water (figure 3*a*, supplementary movie 1), sphere impact into a 1 wt% gelatine pool creates a splash sheet from the air–gelatine interface, which then results in the formation of a surface seal (figure 3*b*, supplementary movie 2). The sphere propagation speed and cavity size are noted to be similar in both the water and 1 wt% gelatine. However, in a more concentrated gel, the cavity elongates and collapses just below the air–gelatine interface, which results in a distinct shallow seal (figure 3*c–e*, supplementary movies 3–5). This event occurs on a much larger time scale (~ 6 ms) in comparison to the surface-seal event (~ 2 ms, figure 3*a,b*). The maximum radius of the cavity R_L decreases as C increases, such that R_L becomes comparable to the sphere radius R in 5 wt% gelatine and less than the sphere radius R in the 10 wt% gelatine. The surface texture of the cavity walls is only visible in weak gelatine, $C \leq 3$ wt% (figure 3*c–d*), while a different pinch-off is noted in the 10 wt% gelatine having a pinch-off depth greater than $0.5H$ (figure 3*f*, supplementary movie 6). In addition, a necked region right above the pinch-off location (Anderson, LaCosse & Pankow 2016) is also noted

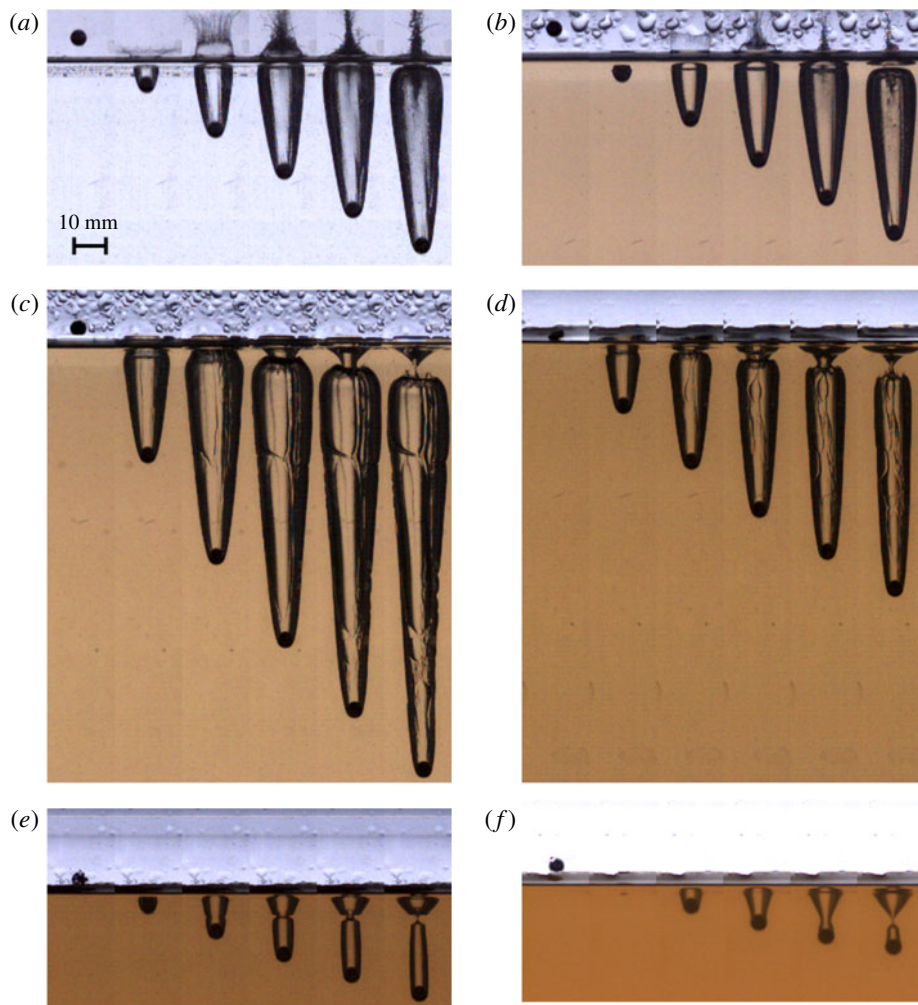


FIGURE 3. (Colour online) Image sequences of cavities in various media with a Froude number of $Fr \sim 4.1 \times 10^5$ and an impact speed of $u_0 \sim 30 \text{ m s}^{-1}$. (a) Surface-seal cavity in water ($\Delta t = 0.4 \text{ ms}$, $We \sim 4.1 \times 10^4$, $Bo \sim 6.8 \times 10^{-1}$), where Δt is the temporal image spacing (also see supplementary movie 1). (b) Surface-seal cavity in 1 wt% gelatine ($\Delta t = 0.4 \text{ ms}$, $Fr_e \sim 1.9 \times 10^4$, $Gr_e \sim 3.3 \times 10^{-1}$, supplementary movie 2). (c) Shallow-seal cavity in 2 wt% gelatine ($\Delta t = 1.2 \text{ ms}$, $Fr_e \sim 4.0 \times 10^3$, $Gr_e \sim 5.5 \times 10^{-2}$). Surface texture is obvious on the cavity wall (supplementary movie 3). (d) Shallow-seal cavity in 3 wt% gelatine ($\Delta t = 0.56 \text{ ms}$, $Fr_e \sim 1.4 \times 10^3$, $Gr_e \sim 2.3 \times 10^{-2}$, supplementary movie 4). (e) shallow-seal in 5 wt% gelatine ($\Delta t = 0.24 \text{ ms}$, $Fr_e \sim 1.9 \times 10^2$, $Gr_e \sim 4.1 \times 10^{-3}$, supplementary movie 5). (f) Quasi-seal cavity in 10 wt% gelatine ($\Delta t = 0.16 \text{ ms}$, $Fr_e \sim 5.9 \times 10^1$, $Gr_e \sim 1.3 \times 10^{-3}$, supplementary movie 6).

in figure 3(c–e). Akers & Belmonte (2006) found that similar necked regions occurred approximately one diameter below the surface and discussed the effects of elasticity and surface tension on the onset. In our experiment, the position of these necks for shallow-seal cases is approximately one or two sphere diameters, which is consistent with the literature. Note, the cavities herein accompanied by the dome-over event

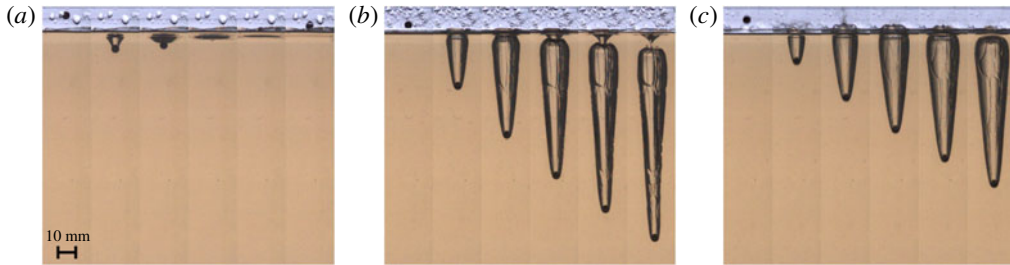


FIGURE 4. (Colour online) Image sequences of cavities in 2 wt% gelatine ($Gr_e \sim 5.5 \times 10^{-2}$) formed by spheres with different impact velocities. (a) Rebound ($u_0 \sim 3 \text{ m s}^{-1}$, $Fr_e \sim 1.8 \times 10^1$, $\Delta t = 8.0 \text{ ms}$, supplementary movie 7). (b) Shallow-seal cavity ($u_0 \sim 30 \text{ m s}^{-1}$, $Fr_e \sim 4.0 \times 10^4$, $\Delta t = 1.2 \text{ ms}$), which is the reproduced version of figure 3(c). (c) Surface-seal cavity ($u_0 \sim 70 \text{ m s}^{-1}$, $Fr_e \sim 1.5 \times 10^4$, $\Delta t = 0.32 \text{ ms}$, supplementary movie 8).

are classified as surface-seal (e.g. figure 3b). Otherwise, cavities where the pinch-off below the air–gelatine interface occurs before the dome-over event are classified as shallow-seal (e.g. figure 3c), even when the overall cavity shape including the opening angle of the cavity is quite similar to that for the surface seal.

Figure 4 shows the effect of impact velocity on cavity formation in 2 wt% gelatine at different u_0 values. In figure 4(a), the sphere does not penetrate the gelatine but, rather, rebounds (supplementary movie 7). Sphere rebound in a similar manner has also been reported in water-entry experiments (Lee & Kim 2008; Speirs *et al.* 2019). In such cases, the inertia of the sphere must exceed the surface tension in order to create a cavity, whereas in gelatine the inertia must overcome the elasticity. In figure 4(b), an increase in the impact speed u_0 leads to the formation of a cavity. Further increase in u_0 introduces the dome-over event and the cavity detachment from the air–gelatine interface (i.e. surface seal, figure 4c, supplementary movie 8).

Similar to water-entry experiments, four different cavity types are observed for impacts with gelatine pools as shown in figure 5. A time series of the impact in gelatine is presented in figure 5(a–d) with the overall shape of the gelatine cavity types at their pinch-off moment (i.e. last frame outlined in various colours). Water-entry cases at the moment of pinch-off are placed next to the last frame of the gelatine cases for comparison purposes, which shows that the two cavity types are quite similar with the exception of the presence of the surface texture and the exact location of the necked region. Digital image extraction of the gelatine and water cases are compared in figure 5(e) to emphasize the similarities between the two cases and, again, reveal that cavity size, surface texture and location of the necked regions are slightly different, but overall can be classified similarly.

More notable differences between gelatine and water-entry cases emerge after the pinch-off events. These are captured in figure 6 showing the (a) surface-seal regime in water, (b) surface-seal regime in 1 wt% gelatine and (c) shallow-seal regime in 3 wt% gelatine pools. The two surface-seal regimes (a,b) exhibit similar behaviours where the first pinch-off occurs near frame 2 and the secondary closure (deep-seal) appears similar in depth, time and shape (frame 3). However, there are two remarkable differences. One is the height of the vertical jet above the surface (i.e. the so-called Worthington jet) from frame 4 to frame 7 where the gelatine jet has a significantly smaller height, due to elasticity. Note that, although the overall volume of the surface dome-over cavity of the $C = 2$ wt% gelatine (figure 4c) is larger than the water case (figure 3a) and 1 wt% case (figure 3b), the accompanying vertical

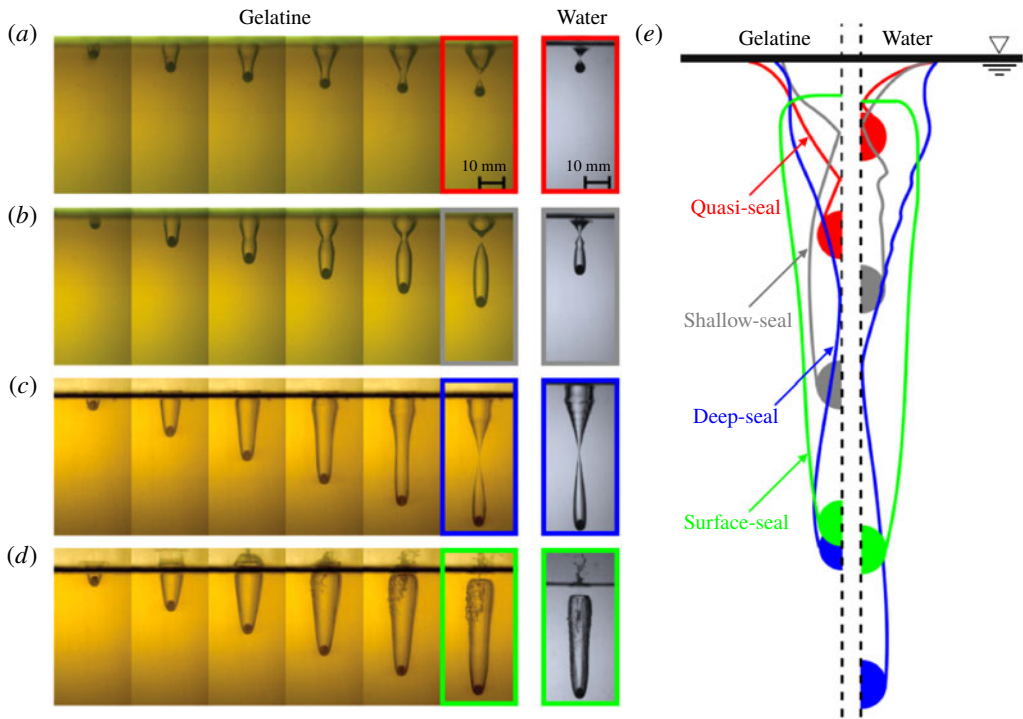


FIGURE 5. (Colour online) The evolution of cavity formation in gelatine for (a) $C = 2$ wt%, $u_0 = 3.4$ m s⁻¹, $Fr_e \sim 2.8 \times 10^1$, $Gr_e \sim 5.5 \times 10^{-2}$, $\Delta t = 1.8$ ms. (b) $C = 2$ wt%, $u_0 = 14.4$ m s⁻¹, $Fr_e \sim 5.2 \times 10^2$, $Gr_e \sim 5.5 \times 10^{-2}$, $\Delta t = 2.0$ ms. (c) $C = 1$ wt%, $u_0 = 2.6$ m s⁻¹, $Fr_e \sim 1.0 \times 10^2$, $Gr_e \sim 3.3 \times 10^{-1}$, $\Delta t = 4.2$ ms. (d) $C = 1$ wt%, $u_0 = 34.2$ m s⁻¹, $Fr_e \sim 1.8 \times 10^4$, $Gr_e \sim 3.3 \times 10^{-1}$, $\Delta t = 1.0$ ms, in comparison with water for quasi-seal (red), shallow-seal (grey), deep-seal (blue) and surface-seal (green) cavity types. The corresponding cavity shape profiles are determined using an edge detection routine and plotted side-by-side in (e) for comparison purposes.

jet has a smaller height. This suggests that the water-like behaviour of the gelatine is suppressed as the gelatine concentration increases. The other is the existence and persistence of bubbles along the path of the cavity a long time after impact. As shown in the far-right panel of figure 6(b) (grey outlined image), the bubbles created by the sphere impact in the gelatine can be trapped for several minutes after cavity closure due to fluid viscoelasticity, while those in the water float upward immediately (not shown). In the shallow-seal case (c), the pinch-off occurs between frames 2 and 3 with the sphere decelerating up to frame 5. The air inside the cavity seems to collapse from the bottom, rising upward except for a small bubble attached to the sphere. The sphere actually moves upward between frames 6 and 8, likely due to elastic recovery (Akers & Belmonte 2006; Mrozek *et al.* 2015). An image taken a few minutes after the impact (figure 6c, grey outlined image) shows a narrow hole (or crack) remaining inside the gelatine along the line of sphere trajectory as proof of its plastic deformation.

An important aspect of this study is that all four cavity types categorized in figure 5 can be produced by particular combinations of C and u_0 . Thus, all five impact phenomena including rebound can be mapped into a phase diagram by

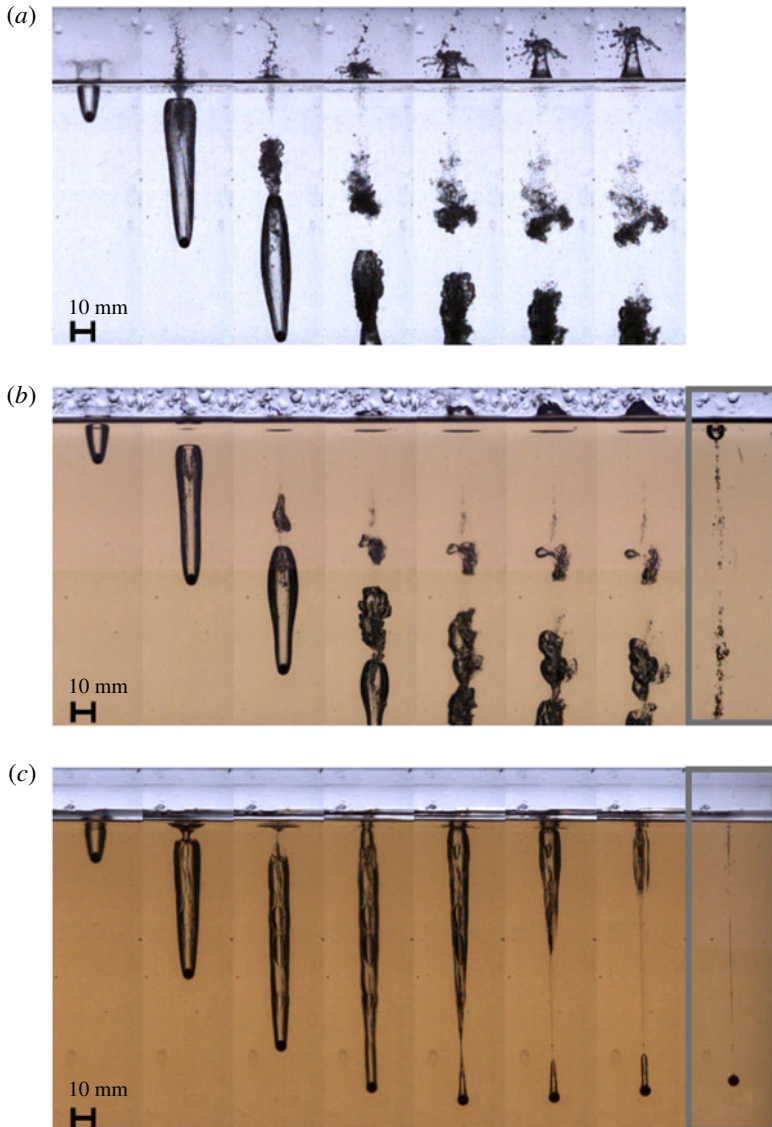


FIGURE 6. (Colour online) Cavity shape after closure. (a) Surface-seal cavity in water ($\Delta t = 2$ ms, reproduced from figure 3a). (b) Surface-seal cavity in 1 wt% gelatine ($\Delta t = 2$ ms, reproduced from figure 3b). (c) Shallow-seal cavity in 3 wt% gelatine ($\Delta t = 2$ ms, reproduced from figure 3d). The last image on the right with a grey outline in panels (b) and (c) is minutes after impact (captured separately) where there are air pockets left open in the wake of the cavity. In (c) the sphere has risen slightly as the cavity closes, likely due to the elastic recovery of gelatine and the now zero inertia of the sphere (supplementary movie 9).

considering the ratio of inertia and gelatine elasticity. In this paper, we use the elastic Froude number Fr_e as a measure of competition between C and u_0 . Although this paper mainly compares cavity dynamics in gelatine with that in water, it is important to point out that the elastic Froude number Fr_e could also be interpreted as a function

of the shear-wave-based Mach number $Ma = u_0/c_s$, where c_s is the speed of the shear wave in gelatine estimated as $c_s \sim \sqrt{G/\rho}$. Based on the definition of Fr_e and Ma , one finds $Fr_e = Ma^2$, indicating that the elastic Froude number Fr_e is not only the ratio of sphere inertia to gelatine elasticity but also the competition between the speed of cavity formation (or surface creation) and the shear wave propagation in the gelatine. Note that the speed of the longitudinal wave in gelatine, which is supposed to be close to that of the compression wave in water, is still much greater than the sphere speed, suggesting that cavity dynamics in gelatine is affected by the shear wave (Rapet, Tagawa & Ohl 2019), where the contribution of the longitudinal wave to cavity dynamics in gelatine is supposed to be comparable to that of the compression wave in water.

4. Discussion

Investigating the cavity length H at cavity pinch-off, figure 7(a) shows a relation between the normalized cavity length $H/(2R)$ versus the elastic Froude number Fr_e . The cavity length H for the quasi-seal, shallow seal and deep seal is measured when the cavity experiences pinch-off below the free surface ($t = \tau$). For surface-seal cases, the cavity length H is measured when the cavity seals at the free surface ($t = t_c$). We use the elastic Froude number Fr_e to classify the cavity types in different gelatine concentrations ($1 \text{ wt}\% \leq C \leq 10 \text{ wt}\%$) into four main regimes, which are highlighted using different shapes. Rebound is noted for smaller Fr_e but once Fr_e exceeds a threshold of $Fr_e \sim O(10)$, the sphere creates a quasi-seal or deep-seal cavity, shallow-seal cavities in the yellow region ($4 \times 10^1 \leq Fr_e \leq 6 \times 10^3$) and surface-seal cavities in the blue region ($Fr_e \geq 6 \times 10^3$). We note that the 1 wt% gelatine acts more like water than an elastic solid. The nearly flat response of $H/(2R)$ to Fr_e (yellow markers) and behaviour like the Worthington jet of figure 3 make it likely that there is a $\tan \delta$ (table 1) threshold that delineates between water-like and elastic-like cavity shapes and sizes.

One may estimate the transition from rebound to quasi-seal by considering the balance of contact pressure p at the sphere impact and shear modulus G . One may assume $p \sim \Delta\rho u_0^2$ for simplicity purposes, which results in the application of a constant Fr_e for cavity formation, consistent with the experimental data presented in figure 7 and those by Swain *et al.* (2014). However, the above oversimplistic estimation (i.e. $G < p$ for the penetration) underpredicts the condition for cavity formation by a decade. It is worth noting that we can predict very different thresholds from the data presented in the literature. For example, a constant $Fr_e \sim 0.1$ is estimated for the ordnance gelatine (Swain *et al.* 2014). On the other hand, estimates for the synthetic polymer gel (Mrozek *et al.* 2015) are found to be $7.4 \times 10^1 \lesssim Fr_e \lesssim 1.3 \times 10^2$. The discrepancy between our data in figure 7 and Swain *et al.* (2014) and Mrozek *et al.* (2015) indicates that the condition for cavity formation is not satisfactorily explained by Fr_e values. Modelling the threshold for cavity formation, possibly as a function of mechanical properties of the gel such as G values, is to be addressed in future work. In this study, the sphere rebound threshold marked by $Fr_e \sim O(10)$ is equivalent to $Ma \sim O(1)$. This might indicate that the speed of the sphere impact is greater than that of the shear wave propagation in the gelatine when the cavity forms.

In shallow-seal cases, a scaling law of the form $H \propto (u_0 - u_{th})/\sqrt{G}$ (Swain *et al.* 2014; Mrozek *et al.* 2015), where u_{th} is the minimum sphere speed required to form the cavity, might be applicable for describing the cavity length H . The relation $H/(2R) \propto \sqrt{Fr_e}$ is thus expected, which indeed follows the data (solid line

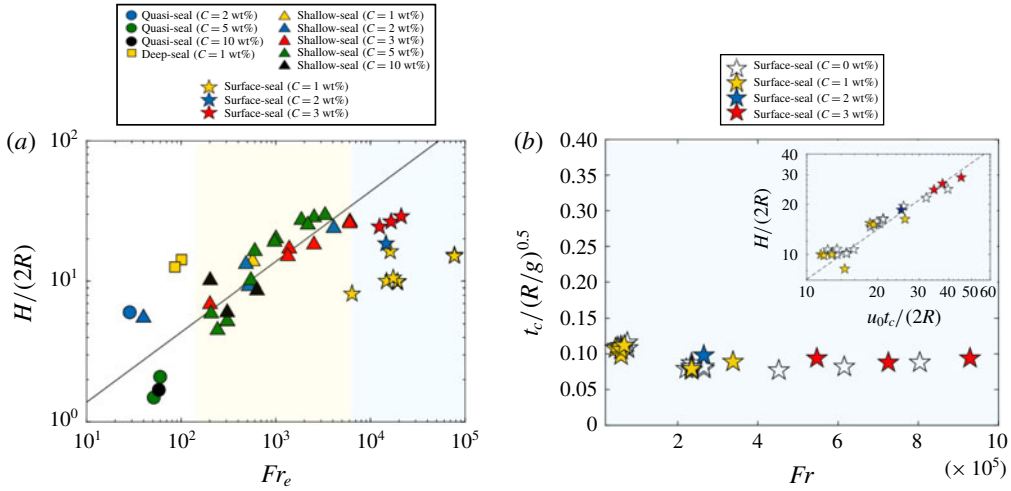


FIGURE 7. (Colour online) (a) Normalized cavity length $H/(2R)$ versus elastic Froude number Fr_e . Solid line indicates the half-power law $H/(2R) \propto \sqrt{Fr_e}$. Coloured areas highlight shallow-seal (yellow region) and surface-seal (blue region) cavities. (b) Normalized time of surface-seal $t_c/\sqrt{R/g}$ for both gelatine (coloured markers) and water (white markers) versus the Froude number $Fr(= u_0^2/(gR))$. The inset shows the normalized cavity length $H/(2R)$ versus $u_0 t_c/(2R)$. Dashed line indicates $H/(2R) = 0.71 u_0 t_c/(2R)$.

in figure 7a). This shows the shallow-seal data and the proposed relation to be in good agreement, suggesting the elastic Froude number Fr_e is a good indicator for describing the length of the shallow-seal cavities.

In the surface-seal regime, the scaling based on the elastic Froude number Fr_e no longer holds; rather, the cavity length ($H/(2R)$) drops as Fr_e increases. Our surface-seal data (figure 7b) indicates that H can be predicted as $H = \alpha u_0 t_c$ (see inset), which assumes a constant sphere propagation speed, regardless of G values. Here $\alpha = 0.71 \pm 0.01$ is the fitting parameter and t_c is the time of surface-seal. This suggests that t_c is also insensitive to G (see also figure 7b), implying that the dynamics of surface-seal cavities is independent of G for the experimental conditions investigated herein. Note that another formulation of the non-dimensional time of surface-seal $t_c u_0/R$ shows Fr dependency within $24 \leq t_c u_0/R \leq 90$ while Marston, Vakarelski & Thoroddsen (2012) reported a constant value ($t_c u_0/R \approx 11.5$) at lower Fr conditions ($200 \leq Fr \leq 1000$). Aristoff & Bush (2009) suggested that the time of surface-seal $t_c u_0/R$ can increase as the Weber number associated with the splash curtain dynamics increases. We also measure the pinch-off time of deep-seal τ after the surface seal. Several empirical relations are reported for deep-seal cavities in water as $\tau = \beta \sqrt{R/g}$, where $\beta = 2.285$ for a disk (Glasheen & McMahon 1996), and $\beta = 1.726$ (Truscott & Techt 2009), $\beta = 1.74$ (Gilbarg & Anderson 1948), $\beta = 2.06$ (Duclaux *et al.* 2007) or $\beta = 2.09$ (Marston *et al.* 2012) for spheres. A significant deviation from these, however, was reported by Mansoor *et al.* (2014) for surface-seal events in an extended Fr regime where the pinch-off time τ decreased significantly as Fr increased. Measuring the time of surface-seal cases for gelatine impacts in this work produces a much smaller empirical value of $\beta = 0.28 \pm 0.03$ found as being less sensitive to G values for the high Fr cases studied herein. Thus, it is

suggested that the pinch-off time τ as well as the surface-seal time t_c in the high Fr limit are remarkably different from those in lower Fr values ($Fr < 1000$). This is possibly due to a stronger reduction in cavity pressure with higher sphere penetration speeds. While the required resolution for studying splash curtain dynamics (e.g. the splash sheet thickness) is beyond the scope of this study, the short-lived nature of these events in extremely high Froude number conditions could be another possible explanation and grounds for future studies.

A phase diagram in the non-dimensional parameter space (Fr_e-Gr_e) is shown in figure 8(a) and a $We-Bo$ plot for water is shown for comparison purposes in figure 8(b). Our water-entry observations are in good agreement with Speirs *et al.* (2019) considering our sphere–water wetting angle is 141° . The relationship between $We-Bo$ and Fr_e-Gr_e here is important as the prior indicates the comparison of sphere inertia and gravity using surface tension (σ/R) while the latter conveys the same information using G in both Fr_e and Gr_e (see table 2). In addition to Fr_e being a good indicator in classifying cavity types, Akers & Belmonte (2006) have shown the transition of cavities to be dependent on Gr_e as well. Well-defined regimes for different cavities are therefore shown in an Fr_e-Gr_e plane (see figure 8) where increasing sphere inertia moves through different cavity types: rebound, quasi-, deep-, shallow- and surface-seal.

There are three main points worth discussing in figure 8: (i) no rebound is observed in water, (ii) a deep seal does not appear to occur in gelatine when $Gr_e \ll 1$ and (iii) a shallow seal occurs between the deep and surface seal in gelatine for increasing Fr_e . In (i), the onset of rebound was not observed in water-entry experiments herein, possibly because of the small contribution of surface tension compared to inertia and gravity. Speirs *et al.* (2019) observed rebound in water-entry experiments only when $We < 0.5$ and $Bo < 0.1$, which are not within range of current experiments. In (ii), at the lowest concentrations of gelatine (largest Gr_e) deep-seal and surface-seal events occur. Yet, at the higher gelatine concentrations, deep-seal and surface-seal events are suppressed. Aristoff & Bush (2009) suggested that the deep-seal regime in water does not exist for $Bo \ll 1$ as hydrostatic pressure, being the driving force for deep-seal events, is dominated by surface tension effects. Similarly, for $Gr_e \ll 1$, the influence of gravity is small compared to gelatine elasticity, resulting in the suppression of deep-seal events therein. While the pinch-off time $\tau = \beta\sqrt{R/g}$, where $\beta = 1.89$ obtained here for water-entry experiments agrees well with previously reported values ($\beta = 1.726$, Truscott & Techet 2009; $\beta = 2.09$, Marston *et al.* 2012), a value of $\beta = 1.42$ obtained in 1 wt% gelatine is slightly smaller in comparison but expected. In (iii), as We increases in water-entry cases, deep-seal events are noted to occur between shallow and surface seals. However, a corresponding increase in Fr_e for gelatine cases results in a deep seal occurring before shallow and surface seals. This is possibly due to the manner in which we classify surface and shallow seals. In our classification a surface dome-over event is a prerequisite for surface seals, which is likely to be suppressed by elasticity in gelatine impact cases (see figures 3 and 4b,c). Maintaining the same classification criteria in both water and gelatine impact cases, cavities in the latter medium can experience suppressed surface dome-over events and hence the discrepancy observed in figure 8.

Although the well-known classification of cavities based on the sealing position in water-entry experiments (Aristoff & Bush 2009) could also be used for categorizing cavities formed in gelatine, they cannot capture all the cavity features perfectly. While the pinch-off location H_p remains constant for different Fr_e conditions (see figure 3c,d), the overall shape of the cavity, which is not only the cavity length H

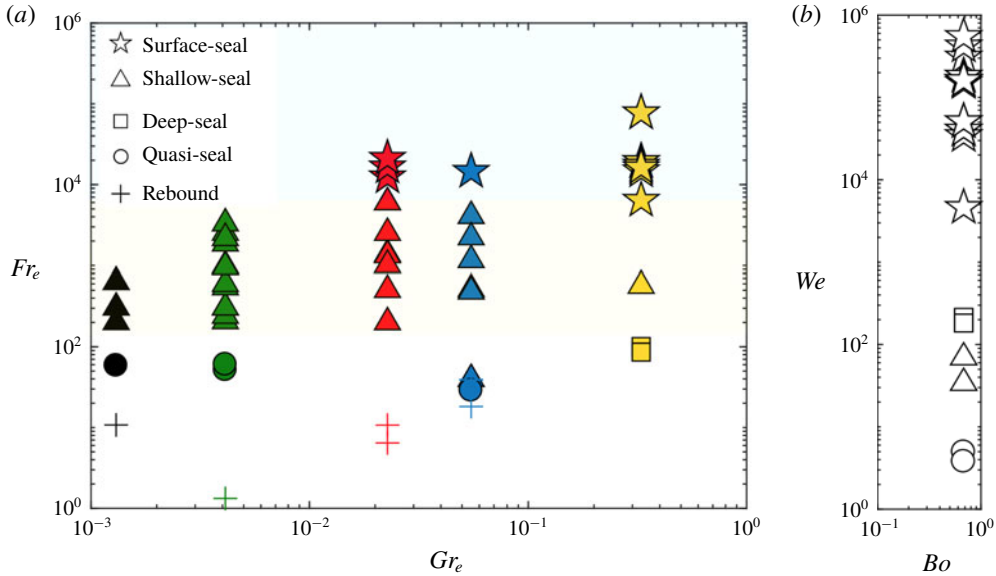


FIGURE 8. (Colour online) (a) Phase diagram for cavity types in an Fr_e – Gr_e plane. The shapes correspond to the cavity types. The colours indicate the concentration of gelatine as shown in figure 7. (b) The four different cavities observed in water are presented by white markers in the We – Bo plane.

but also the maximum radius of the lower cavity R_L , is dependent on Fr_e values. Thus, in order to understand the cavity features in gelatine more comprehensively, we focus on the overall cavity shape in figure 5(e) and figure 9. Figure 9(a) presents the normalized pinch-off location H_p/H where the well-known quasi-seal and deep-seal cavities are categorized by $H_p/H > 0.5$ and $H_p/H \sim 0.5$, respectively. For the shallow-seal cases, H_p/H decreases as Fr_e increases because the cavity length H increases while H_p remains relatively constant (figure 3). Higher Fr_e introduces surface-seal cases, where $H_p/H = 0$. Note that H_p for surface-seal cases is measured when the splash crown seals at the free surface occurs ($t = t_c$). Here we also compare the non-dimensional pinch-off location H_p/R for shallow-seal cases of both water and gelatine in order to confirm that the pinch-off location H_p is independent of the sphere impact speed. Aristoff & Bush (2009) derived a constant H_p/R for a fixed contact angle and confirmed experimentally that the measured value was slightly correlated with the sphere impact speed up to $H_p/R < 5$. Our water-entry data ($H_p/R < 2.7$) agrees fairly well with their assessment. Similarly, our gelatine data shows the relatively constant pinch-off location H_p/R (see inset of figure 9a), where the mean value and the standard deviations are $H_p/R = 3.38 \pm 0.66$. The maximum radius of the lower cavity R_L/R increases as Fr_e increases (figure 9b). As discussed in figure 7(b), the cavity dynamics in gelatine for surface-seal events is quite similar to that in water, and is insensitive to G values. Thus, any clear relation between R_L/R and Fr_e is not observed for surface-seal in figure 9(b).

While the dynamics of surface-seal cavities has not been explored in past literature with excessive detail, the fluidic behaviour that is reported is quite similar to our findings. Veyssset *et al.* (2018) showed that the impact of a copper microparticle at 435 m s^{-1} can cause surface dome-over at the surface of a protein hydrogel.

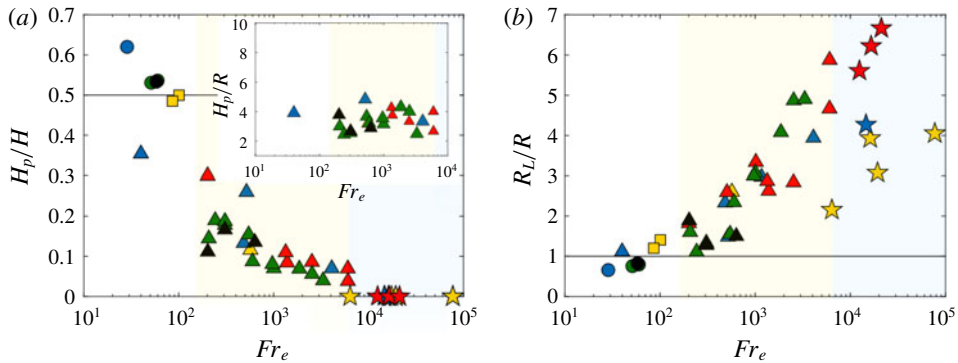


FIGURE 9. (Colour online) The overall pinch-off and shape characteristics for all cavity types. The colour and shape indicate gelatine elasticity and cavity types as in figure 7. (a) Normalized pinch-off height H_p/H versus elastic Froude number Fr_e . Solid horizontal line indicates $H_p/H = 0.5$. The inset shows the normalized pinch-off height H_p/R for shallow-seals as a function of the elastic Froude number Fr_e . (b) The normalized maximum cavity radius R_L/R versus elastic Froude number Fr_e . Solid horizontal line indicates $R_L/R = 1.0$.

Their maximum radius R_L/R is found to be $R_L/R \approx 5$, which is comparable to that obtained from our surface-seal data. We estimate the elastic Froude number $Fr_e (= \rho u_0^2/G)$ for Veysset case as $Fr_e \sim 4.7 \times 10^4$ based on the rheological data for the protein gel as ($G \sim G' \sim 4.0 \times 10^3$ Pa, Olsen, Kornfield & Tirrell 2010). While this is consistent with Fr_e values for the surface-seal regime in figure 8, the elastic Grashoff number Gr_e is not within range. Note that Veysset *et al.* (2018) showed that surface dome-over does not occur when a lighter particle (silica sphere, $\rho_s \sim 1850$ kg m $^{-3}$, $R \sim 3.7$ μ m) impacts the same gel at a faster velocity (~ 530 m s $^{-1}$). Further studies are hence warranted investigating the dome-over phenomenon in viscoelastic fluids in more detail.

5. Conclusion

This study investigates the dynamics of cavity formation when a sphere impacts onto a deep gelatine pool. The cavities were filmed using high-speed imaging and generally found to be affected by both impact velocity u_0 and gelatine elasticity G significantly. The uniqueness of gelatine cavities in terms of shape and structure, including the formation of streaks on the cavity wall, were also outlined in comparison with those obtained in water. To understand the complex cavity dynamics in gelatine, we classify ‘cavity types’ in a non-dimensional Fr_e – Gr_e space analogous to the *We*–*Bo* classification in water-entry cavities (Aristoff & Bush 2009; Speirs *et al.* 2019). The normalized cavity length $H/(2R)$ is an important parameter which can be scaled by the elastic Froude number Fr_e , especially in shallow-seal cases. In addition, while the normalized pinch-off depths H_p/H ratios decrease, the maximum radius of the lower cavity R_L/R increases with increasing Fr_e . The only exception occurs for surface-seal events (in the latter case) which are found to exhibit cavity dynamics insensitive to the shear modulus G and somewhat similar to that observed in water.

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Supplementary movies

Supplementary movies are available at <https://doi.org/10.1017/jfm.2019.696>.

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