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NOTE.—As far as possible, the country of origin quoted in the items refers to the original source.

LIST OF ABBREVIATIONS OF TITLES AND JOURNALS.

A.	Abstracts from the Scientific and Technical Press.
Aeron. Eng.	Aeronautical Engineering (U.S.S.R.)
Aer. Res. Inst. Tokyo	Aeronautical Research Institute of Tokyo.
A.C.I.C.	Air Corps Information Circular.
Ann. d. Phys.	Annalen der Physik
Army Ord.	Army Ordnance.
Autom. Eng.	Automobile Engineer
Autom. Ind.	Automotive Industries.
Autom. Tech. Zeit.	Automobile Technische Zeitschrift.
Bell Tele. Pubs.	Bell Telephone Publications.
Bur. Stan. J. Res.	Bureau of Standards (U.S.A.) Journal of Research.
Chem. Absts.	Chemical Abstracts.
Chem. and Ind.	Chemistry and Industry.
Comp. Rend.	Comptes Rendus de L'Académie des Sciences.
Eng. Absts.	Engineering Abstracts.
E.N.S.A.	Revue Technique de l'Association des Ingénieurs de l'Ecole Nationale Supérieure de L'Aéronautique.
Forschung	Forschung auf dem Gebiete des Ingenieurwesens.
Fuel	Fuel in Science and Practice.
H.F. Technik.	Hochfrequenztechnik und Electroakustik.
Ind. and Eng. Chem.	Industrial and Engineering Chemistry.
Ing.-Arch.	Ingenieur-Archiv.
Inst. Autom. Eng.	Institute of Automobile Engineers (Research and Standardisation Committee).

J. Aeron. Sci.	Journal of the Aeronautical Sciences.
J. App. Mech.	Journal of Applied Mechanics.
J. Am. Soc. Nav. Eng. ...	Journal of American Society of Naval Engineers.
J. Roy. Aero. Soc.	Journal of Royal Aeronautical Society.
J. Frank. Inst.	Journal of Franklin Institute.
J. Inst. Civ. Eng.	Journal of Institute of Civil Engineers.
J. Inst. Elec. Eng.	Journal of Institute of Electrical Engineers.
J. Inst. Petrol.	Journal of the Institute of Petroleum.
J. Met. Soc.	Journal of Meteorological Society.
J. Sci. Inst.	Journal of Scientific Instruments.
J.S.A.E.	Journal of Society of Automotive Engineers.
J. Soc. Chem. Ind. (Abstracts B)	Journal of the Society of Chemical Industry (British Chemical Abstracts B)
L'Aéron.	L'Aéronautique.
L.F.F.	Luftfahrt-Forschung.
Luschau.	Luftfahrt-Schrifttum des Auslandes
Met. Mag.	Meteorological Magazine.
Met. Prog.	Metal Progress.
N.A.C.A.	National Advisory Committee for Aeronautics (U.S.A.).
Phil. Mag.	Philosophical Magazine.
Phil. Trans. Roy. Soc. ...	Philosophical Transactions of the Royal Society.
Phys. Berichte.	Physikalische Berichte.
Phys. Zeit.	Physikalische Zeitschrift.
Proc. Camb. Phil. Soc. ...	Proceedings of Cambridge Philosophical Society.
Proc. Inst. Rad. Eng. ...	Proceedings of Institute of Radio Engineers.
Proc. Roy. Soc.	Proceedings of Royal Society.
Pub. Sci. et Tech.	Publications Scientifiques et Techniques du Ministère de l'Air.
Q.J. Roy. Met. Soc.	Quarterly Journal of the Royal Meteorological Society.
R. and M.	Reports and Memoranda of the Aeronautical Research Committee.
Rev. de l'Arm. de l'Air ...	Revue de l'Armée de l'Air.
Riv. Aeron.	Rivista Aeronautica.
Sci. Absts. (A. or B.) ...	Science Abstracts (A or B.).
Sci. Am.	Scientific American.
Sci. Proc. Roy. Dublin Soc.	Scientific Proceedings of Royal Dublin Society.
Tech. Aéron.	La Technique Aéronautique.
Trans. A.S.M.E.	Transactions of the American Society of Mechanical Engineers.
Trans. C.A.H.I.	Transactions of the Central Aero-Hydrodynamical Institute, Moscow.
U.S. Nav. Inst. Proc. ...	U.S. Naval Institute Proceedings.
Veröffentl. (Siemens) ...	Veröffentlichungen aus dem Gebiete der Nachrichtentechnik (Siemens).
W.R.H.	Werft Reederei Hafen.
W.T.M.	Wehrtechnische Monatshefte.
Z.A.M.M.	Zeitschrift für Angewandte Mathematik und Mechanik.
Z.G.S.S.	Zeitschrift für Das Gesamte Schiess und Sprengstoffwesen mit der Sonderabteilung Gasschutz.
Z. Instrum.	Zeitschrift für Instrumentenkunde.
Z. Mech.	Zentralblatt für Mechanik.
Z. Metallk.	Zeitschrift für Metallkunde.
Z.V.D.I.	Zeitschrift des Vereines Deutscher Ingenieure.

Some Notes on the Ideal Efficiency of Airscrews. (W. Hoff, L.F.F., Vol. 18, No. 4, 22/4/41, pp. 114-121.) (91/4 Germany.)

According to the simple jet theory, the thrust is distributed uniformly over the actuator disc and there are no rotary losses. If the disc is replaced by rotating blade elements, rotary losses cannot be avoided. If it were possible to operate the blade elements at different angular velocities so that ω_r is constant along the blade, the axial losses distributed uniformly over the jet would remain unchanged and the additional rotary losses are also distributed uniformly. Such an arrangement has the greatest possible efficiency. In practice, however, the blade elements necessarily operate at constant ω irrespective of r , and the best thrust distribution with smallest losses is achieved when the induced efficiency of the ring elements varies between an inner and an outer limit. The author compares the resultant efficiency with the ideal case (ω_r constant) and notes a small loss, necessarily associated with the high v/u ratio for elements near the hub (v =translatory and u =circumferential speed).

In conclusion the author's results are compared with other theoretical investigation on lightly loaded propellers and in this connection extensive references are made to Glanert's article on "Airplane Propellers" in Vol. IV of Durand's "Aerodynamic Theory."

Dornier Do 18 Flying Boat Fitted with B.M.W. 132 Air-cooled Radial Engines. (Luftwissen, Vol. 7, No. 12, Dec., 1940, pp. 420-422.) (91/5 Germany.)

The Dornier flying boat was originally fitted with two liquid-cooled Diesel engines (Jumo 205) arranged in tandem on the central section of the wing surface, the front engine being fitted with a tractor airscrew, whilst the rear engine operates a pusher screw through an extension shaft. This arrangement provided small frontal resistance, high efficiency of the pusher screw and good performance when flying on one engine only. Moreover, the Diesel engines had a very small fuel consumption and this contributed to the exceptional range of the boat (record flight of 8,400 km.). With the coming of the war, increasing use was made of the machine for flight of relatively limited range. At the same time, the need for a catapult start was felt to be a drawback. Both these requirements were met by replacing the Jumo engines with 2 B.M.W. radials arranged in tandem as before and completely immersed in one engine nacelle. In this arrangement air enters the front engine in the normal manner through the centre of the cowl and is exhausted through two lateral and controllable ports in the nacelle immediately behind the engine. The cooling air for the rear engine enters a scoop at the rear of the nacelle, is turned through 90° and fed to a cooling fan. The air then impinges on the exhaust side of the rear engine (which is mounted in the reverse direction to the front engine) and after passing the engine is exhausted through a second pair of lateral ports placed behind the first pair. The cooling air stream to the second engine thus moves in a direction opposing that of flight. The two sets of lateral ports are so positioned that no hot air can enter the rear scoop. It is stated that the cooling of both engines is satisfactory and that the assistance of the fan provides sufficient cooling even if the rear engine (working the pusher airscrew) is operated alone.

The performance of the boat has been vastly improved since the change in engines. Whilst before an all up weight of 10 tons required a catapult start, weights up to 13.5 tons have been lifted without take-off assistance. In spite of the power absorbed by the cooling fan, the increased efficiency of the pusher screw is such that, for single engine take-off, the rear engine alone will lift 400 kg. more than the front engine.

The relative power outputs of the old and new engines is given in the following table:—

	Take-off h.p.	Cruising h.p.	Sp. fuel consumption gm./b.h.p. hour.	Weight/power ratio kg./h.p.
Junno 205 ...	600	510	165	0.87
B.M.W. 132...	850	630	215	0.56

Material Investigations on Steel Fittings and Structural Parts of Some Captured British, American and French Aircraft. (H. Cornelius, Luftwissen, Vol. 8, No. 3, March, 1941, pp. 78-81.) (91/6 Germany.)

The steel parts examined were taken from the following aircraft:—

British: Blenheim, Wellington, Hampden, Battle, Spitfire.

U.S.A.: Hudson.

France: Morane, Lioré-Olivier.

And covered wings, fuselage, engine supports, landing gear and armour plating.

Attention is called to the extensive use of high alloy Ni-Cr-Mo steels by the British and French. According to the author, equivalent performance can be obtained without Ni, and the resulting Cr-Mo steels have the additional advantage

of being weldable. This is the German and also the American practice. It appears that welding is still not favoured by the British designer. British armour plate varies in thickness from 4.3 to 9.3 mm., with high Ni content (3.1 to 3.9 per cent.). The Fairey Battle used a non-magnetic Mn steel which is totally unsuitable for armour plating on account of its brittleness under bullet impact.

Automatic Riveting in Aircraft Construction. (C. H. Plock, *Luftwissen*, Vol. 8, No. 2, Feb., 1941, pp. 36-42.) (R.T.P. Translation No. 1,190.) (91/7 Germany.)

The article deals with flush riveting as practiced by the Focke-Wulf Company. Such rivets can either be of the mushroom or flat head type. In the former, the rivet is inserted from the inside and the countersunk head produced from the rivet shaft, previously cut to the exact length to produce a flush fit in the dimpled sheet. The flat head rivet is inserted from the outside, the closing head being produced on the inside without requiring exact dimensioning of rivet length. In plates over 1.2 mm. thickness, the countersink is normally produced by a special tool akin to a milling cutter, the operation being usually combined with the drilling of the rivet hole. For thinner plates, the necessary deformation of the countersink is produced mechanically (dimpling) either by the rivet itself or by means of special tools. If a thin outer skin is to be attached to a thicker plate, the latter is machine countersunk whilst the former is pressed to shape again either by the rivet itself or by a special tool prior to insertion of the rivet. Dimpling by means of the rivet is more economical, but the special tool furnishes a smoother surface. In the simple riveting machine, the operation is limited to the closing of the rivet, either by gradual pressure (air, oil, or a combination), a single blow or multiple blows. A semi-automatic riveting machine combines insertion with dimpling and clenching in one operation. An "automatic" riveter includes drilling the hole, whilst a fully automatic machine also incorporates a work feed. It is also possible for the machine to manufacture the rivets as wanted by cutting off suitable lengths of wire carried on a reel. Representative type of semi and fully automatic machines are illustrated, and an interesting optical device for facilitating alignment of rivet with previously drilled holes is described.

Whilst the simple closing press requires but little operative skill, automatic riveting machines are much more delicate and trained personnel is essential. In the author's opinion, however, the saving in time is such that the high first cost of the automatic is well worth while.

Efficient Design. (*Luftwissen*, Vol. 8, No. 2, Feb., 1941, pp. 48-49.) (91/8 Germany.)

In the past, production has been increased by employing more labour and working longer hours. Much can, however, be done by efficient design, which not only makes the labour more productive but also saves valuable material. Thus the Dornier works make considerable use of welded steel fittings for wings. Previously such fittings were made of die forgings, and in an example illustrated the original forging weighed 0.65 kg. reduced to 0.28 kg. after machining. By altering the design so that the flange consisted of two portions welded together, the quantity of material required was reduced to 0.20 kg. whilst the time taken to produce the finished article was 40 per cent. less. Tests have conclusively proved that such welded fittings are fully equal to the original product machined out of the solid. Another big saving in time and material can be brought about by the substitution of pressings for previously riveted wing ribs.

It is stated that by introducing 30 small design improvements of this type in a certain aircraft, 90 man hours were saved in labour and the finished machine weighed 42 kg. less, combined with a further saving of 64 kg. in material utilised.

The Influence of Bending and Buckling on Stress Measurements Carried Out on Shell Structure of which Only One Side is Accessible. (A. Dose, L.F.F., Vol. 18, No. 2-3, 19/3/41, pp. 95-101.) (91/9 Germany.)

Stress calculations based on extensometer measurements carried out on the surface of stressed skins can be seriously affected by the even slight buckling of the skin. The corresponding extension due to bending can be eliminated if extensometer measurements are carried out on both sides of the skin. In many cases, however, the interior of the structure is not accessible and it is important to estimate the necessary correction by means of measurements confined to the outer surface.

On the assumption that the bulge is of circular shape, the corresponding strain $\epsilon = d/2 \times 1/R$ where d = thickness of skin and R = radius of curvature of the neutral fibre. The latter can be determined by measuring the height f of the bulge above a chord of length s . Provided f is small and $df/(s/2)^2 < 1$,

$$\epsilon = \frac{df}{(s/2)^2}$$

to a high degree of accuracy.

It is obvious that f can be measured by means of a suitably geared mechanical pointer similar to the spherometer employed in lens measurements and the author has incorporated such a device in the standard Huggenberg extensometer. In this case the extensometer base line coincides with the chord for the f measurements and corrections have to be applied to the strain determination in order to take into account the change in chord length with buckling. These corrections are tabulated by the author. The effect of a bulge of varying curvatures is also investigated. It appears that such changes can generally be neglected if the base line is less than 20 mm. in length. In conclusion, the author gives an example of the effect of buckling on stress distribution in the web of wing spar. (Light alloy skin, 0.75 mm. thick.) The table summarises the results.

	Uncorrected.	Ditto, corrected for buckling.
Principal stress σ_1 ...	-1060 kg./cm. ²	-678 kg./cm. ²
σ_2 ...	+460 kg./cm. ²	+558 kg./cm. ²
τ_{max} ...	760 kg./cm. ²	618 kg./cm. ²
α ...	-36.4°	-37.5°

The Landing Process (Length of Run, Braking Effort and Possibility of Tipping Over). (G. Matthias and R. Schaeff, L.F.F., Vol. 18, No. 2-3, 29/3/41, pp. 70-76.) (91/10 Germany.)

The principal object of the author is to determine the factors controlling the landing energy which must be absorbed by the brakes. The danger of tipping (nosing) over is also investigated. Other things being equal, the length of landing run varies as the square of the touch down speed. The principal factors influencing the run are the air resistance, weight, ground friction and brake operation. If a maximum length of run is stipulated for a given wing area and lift coefficient, the kinetic energy to be absorbed by the brakes varies as the square of the aircraft weight (fourth power of landing speed), besides depending on the air forces and friction coefficients during the run. The ratio of lift coefficients at touch down and during rolling on the ground is of primary importance and requires careful consideration when comparing the landing properties of nose wheel and tail wheel aircraft. Even if the brake operation is not limited by the heat generated, the possibility of nosing over puts an upper limit to its braking effort. Nosing over will occur if the ratio (total frictional force)/(weight) becomes greater than the tangent of the angle between the vertical and the line joining the point of contact of the main landing wheels with the C.G. of the aircraft. At the beginning of the run, the lift reduces the effective retarding forces and the danger of nosing over thus only arises towards the

end of the run. The shortest landing run is obtained if the brakes are fully on at touch down and then gradually released so that (retarding force)/(weight) is always just smaller than the tangent of the above mentioned angle.

In the German Safety Regulation for Aircraft, the minimum value of this angle is fixed at 12° for the most forward position of the C.G., the longitudinal axis of the aircraft being assumed horizontal. According to the author this should be modified to cover the fuselage altitude corresponding to three-point landing.

Rate of Vertical Descent after Flattening Out Prior to Landing. (J. Carsens and H. Schaeffer, L.F.F., Vol. 18, No. 2-3, 29/3/41, pp. 77-81.) (91/11 Germany.)

The aircraft is assumed to be moving horizontally at a velocity v_0 so that

$$v_0^2 = G/c_a (\rho/2) F$$

where c_a = lift coefficient.

G = weight.

F = wing area.

There is no propeller thrust and the subsequent motion of the C.G. is investigated on the assumption that the angle of incidence remains constant, i.e., c_w/c_a is independent of the path angle γ (c_w = drag coefficient).

The resulting equations of motion are integrated by the step by step method with the help of auxiliary functions and the rate of vertical descent v_z after a loss of altitude z as well as the corresponding path distance s along the trajectory are expressed graphically as functions of v_0 and z with c_w as parameter. For the practical range c_a at which flattening out should take place, the expression

$$v_z = \sqrt{\frac{c_w}{c_a} 2gz}$$

holds with good approximation. The actual rate of descent does not increase indefinitely with z , but oscillates with gradually decreasing amplitude about a terminal value. A worked out example for the Fw. 159 aircraft gives the following results:—

$$\left. \begin{array}{l} G = 2,250 \text{ kg.} \\ F = 20.2 \text{ m.}^2 \\ c_w/c_a = 0.152 \\ c_a = 1.70 \\ v_0 = 31 \text{ m./sec.} \end{array} \right\} \text{Flaps down, landing wheels out.}$$

z	v_z	s
2	2.3	72
4	3.5	95
8	5.0	120
12	5.7	130
20	6.6	175
28	7.4 (max.)	202
36	7.0	270
40	6.6	260
50	4.8	318
~ 150	4.6 (terminal)	—

Dynamic Balancing of Airscrews. (Escher Wyss, Inter. Avia., No. 754-55, 15/3/41, pp. 10-11.) (91/12 Switzerland.)

The Escher Wyss Maschinenfabriken A.G., of Zurich, Switzerland, carry through the dynamic equilibration of their airscrews on a new type of test bench on which the airscrew is attached on a cantilever mount and supported on one side only. As a result, undisturbed flow conditions such as prevail around the

airscrew mounted on the aeroplane are obtained and sources of error of conventional equilibration benches eliminated. The aerodynamic unbalance of the airscrew may be of the same magnitude as the mechanical unbalance caused by weight differences, the position of the axis and the blades' centre of gravity paths and is caused: (1) By small irregularities in the finish of the airscrew blades as well as the latter's angle of incidence. This type of unbalance could be separated from the mechanical type only by test runs in a vacuum chamber; together the two types result in a sinuous form of oscillation. (2) By the surroundings of the airscrew, *i.e.*, by irregularities in the air flow. The disturbances in the air flow in the vicinity of the airscrew cause, besides the fields of vorticity not depending upon the airscrew speed, pressure shocks every time a blade passes through the disturbed region; these shocks result in an oscillation corresponding to the number of blades and superimposed on the sinuous oscillation. These interfering oscillations may assume such a magnitude as to prejudice the calculation of the measuring results. The oscillations are measured by Escher Wyss not by mean value calculation but by direct optical observation, which provides a very reliable means of determining dynamic unbalances even in the region of great interference amplitudes.

Permanent Buckling Stress of Thin Sheet Panels Under Compression. (W. L. Howland and P. E. Sandorff, *J. Aeron. Sci.*, Vol. 8, No. 7, May, 1941, pp. 261-269.) (91/18 U.S.A.)

In this report it has been shown that:—

1. The problems of skin buckles are of increasing importance to the airplane designer, particularly with high design stresses, low design load factors and greater aerodynamic efficiency.
2. The computed critical buckling stress has practical significance only once in the history of the structure.
3. Structure which buckles in service should be designed so that it will be free of objectionable buckles at a load factor of from 1 to 1.25 after the application of maximum anticipated service load.
4. Theoretical computations indicate a relation between the maximum stiffener stress for objectionable buckling and the critical buckling stress, and this relation is substantiated by experimental data.
5. In applying data on skin buckles to the design of monocoque structures, it is necessary to determine the relation of the stress at maximum service load to that at a load factor of 1.25. This can be expressed through a ratio of panel loads. For buckling materials, an accurate value of panel load is obtained through the use of van Kármán's effective width relation.
6. The relation of the maximum stiffener stress to the critical stress for objectionable buckling can be expressed by a family of curves as in Figs. 9 and 10.

Directional Stability and Vertical Surface Stalling. (G. S. Schairer, *J. Aeron. Sci.*, Vol. 8, No. 7, May, 1941, p. 270.) (91/19 U.S.A.)

A vertical tail stall can only be obtained by yawing the aeroplane to angles at which fin stalling or rudder force reversal or both are obtained. This seldom occurs at less than 15° of yaw. Large aeroplanes are never yawed to any appreciable extent in normal operation and vertical tail stalls are never encountered in normal operation. On some classes of aeroplanes the use of the sideslip manoeuvre is desirable, but even on these aeroplanes the sideslip angles normally used would not ordinarily produce a tail stall. Multi-engined aeroplanes, when operated with unsymmetrical power, are frequently flown with some yaw or sideslip, but even then the angle of yaw normally used will not produce a tail stall. There are probably only three ways in which an aeroplane is likely to be yawed sufficiently to produce a tail stall. These are as follows:—

1. Inadvertent engine failure at extremely low speeds on multi-engined aeroplanes on which the rudder is either incapable of supplying all the required restoring moment, or its action is delayed by the human element.
2. Inadvertent excessive sideslipping of manoeuvrable aeroplanes.
3. Intentional excessive sideslipping for experimental, educational and other reasons.

On the original version of the Stratoliner at an angle of yaw of about fifteen degrees a noticeable reversal in the pedal force required to produce yaw was measured. This was as noticeable under symmetrical conditions as with one engine dead. The wind tunnel tests of this configuration showed no evidence of a fin stall, but did show a marked loss in stability with the rudder free at between ten and fifteen degrees of yaw.

A new tail surface including a dorsal fin was fitted to the machine and extensive flight tests carried out. At ninety miles per hour with the engines operating at take-off power, the left outboard engine was suddenly throttled. No rudder correction was made and equilibrium in yaw was reached at thirty degrees of yaw. The aeroplane has been flown with both left-hand engines throttled and the right engines at rated power at speeds below 85 miles per hour at zero yaw.

Adequate directional stability has been demonstrated repeatedly by simulating an engine failure during a landing approach with flaps full down at speeds below 85 miles per hour. While in this condition, the throttles on all engines except the left outboard engine are opened, the aeroplane is placed in a climb, and the landing approach abandoned. This is probably the supreme test for any aeroplane. A four-engine aeroplane would be a little safer than a two-engine aeroplane if it did not have the directional stability and control characteristics necessary to make such a manoeuvre.

The Stressing of Circular Frames in Shell Structures. (H. Fahlbusch and W. Wegner, L.F.F., Vol. 18, No. 4, 22/4/41, pp. 122-127.) (91/20 Germany.)

The author investigates the stress distribution for frames of constant bending stiffness under four fundamental load conditions:—

- A. Localised radial force acting on the frame.
- B. Localised moment acting along a diameter of the frame.
- C. Localised tangential force acting along the neutral fibre of the frame at a distance r from the centre.
- D. Localised tangential force acting along the outer periphery of the frame at a distance R from the centre (=distance of shear flux in shell from centre).

The distribution of bending moment, normal and lateral forces are given in a series of diagrams.

Any arbitrary load can be built up from the above standard cases and the resultant stress distribution obtained by superposition, provided that:—

1. The depth of the circular frames is small compared with r .
2. The cross-section remain plane.
3. The influence of the longitudinal and lateral force on the displacement factors can be neglected.
4. The bending stiffness of the shell is small compared with that of the frame.
5. The frames remain practically circular.

A worked out example illustrates the method.

Aerodynamic Forces Acting on the Wing-Aileron-Tab Combination when Undergoing Harmonic Vibration. (F. Dietz, L.F.F., Vol. 18, No. 4, 22/4/41, pp. 135-141.) (91/21 Germany.)

This is an extension of a previous paper by the author published in L.F.F., Vol. 16 (1939), pp. 87-96, and which covered the two-dimensional case of the

wing-aileron-tab on the supposition that the leading edge of both aileron and tab coincide with the axis of rotation. The formulæ already obtained are reformed so as to apply to the case of aerodynamic balanced surfaces, portions of the equivalent doubly hinged flat plate in front of the hinges, thus forming part of the aileron and tab respectively. These hinges, of course, will not in general coincide with the axis of rotation of either aileron or tab. This conception seems permissible provided the gap between wing and aileron or aileron and tab is small and that the total wing profile is not much affected by the deflection of aileron and tab.

Expressions for the resulting aerodynamic forces are given in tabular form, the use of which is illustrated by a worked out example. The case of a wing aileron combination undergoing harmonic vibrations varying between 0 and 160/sec. at airspeeds of 80 and 160 m. per sec. respectively is considered for two cases of hinge position, (a) hinge coincides with leading edges of aileron, (b) axis of rotation of aileron is situated at 1/5 chord behind leading edge. It appears that the reduction in aerodynamic moment with displacement of axis of rotation is practically independent of vibration frequency or air speed.

Design of Blade Feet for Airscrews. (G. Cordes, L.F.F., Vol. 18, No. 4, 22/4/41, pp. 128-134.) (91/22 Germany.)

The stressing of modern airscrews is steadily increasing due to the large h.p. employed and the increasing utilisation of the airscrew as a brake during high speed power dives. Not only must the hub be strong enough to carry the heavy loads, but even small deformations must be avoided as they may cause difficulties in the operation of the pitch changing mechanism. In addition the blade feet are subjected to a combination of static and dynamic load requiring careful investigation. The alternating stresses constituting the dynamic load are mainly induced by the engine torque variation, whilst the static load (combination of centrifugal and aerodynamic forces) depends on the operative conditions of the airscrew (take-off, normal flying, driving with engines throttled or full power dives with airscrew acting as a brake).

If

- S_o = static thrust of complete propeller,
- M_d = mean engine torque,
- z = number of blades,
- S = thrust per blade,
- T = circumferential force per blade at $0.7 R$,

we have

$$S = sS_o/z$$

$$T = t \frac{M_d}{0.7 Rz}$$

when s and t are factors depending on operative conditions.

In addition we have:—

$$M_{dw} = aM_d$$

where M_{dw} = torque fluctuation at propeller shaft and a = constant depending mainly on the damping in the circuit. With the use of D.V.L. data on fatigue limits, the author works out minimum blade feet diameters as a function of h.p. absorbed for blades made of dural, electron and wood respectively.

Four different operative conditions are considered in each case corresponding to take-off and power dives for two values of the torque fluctuation, the corresponding values of the constants being given below:—

Case.	a	s	t
1	± 0.5	1	1
2	± 0.5	2	1
3	± 1.0	1	1
4	± 1.0	2	1

(1) and (3) correspond to take-off; (2) and (4) are power dives with propeller acting as a brake.

$a = \pm 1.0$ is representative for current engine installations; the smaller value of "a" can be obtained by efficient damping.

The results are given in a series of curves, from which the following values have been extracted for load case 3.

		H.P. absorbed by complete propeller.			
		Wood.	Electron.	Dural.	
Effective blade foot diameter	140 mm.	$z=3$	1150	1400	1600
		4	1430	1700	2000
		5	1700	2000	2500
Effective blade foot diameter	160 mm.	$z=3$	1560	1850	2300
		4	1960	2300	2850
		5	2340	2750	3400

On the supposition that the hub is sufficiently strong the safe h.p. during a power dive with the airscrew acting as a brake is only 10 per cent. less than the figure given.

Reducing (a) from ± 1 to ± 0.5 , increase the safe h.p. by about 50 per cent. under take-off conditions, but by only 20 per cent. when using engines as a brake during power dives.

Speaking generally, a propeller designed for take-off conditions will not absorb the same power when acting as a brake during a dive, unless either the number of blades or the blade foot diameter is increased.

From the point of view of production, the latter alternative is recommended.

Material and Design of Some Captured British, American and French Aero Motors. (P. Kotzschke, Luftwissen, Vol. 8, No. 3, March, 1941, pp. 69-78.) (91/23 Germany.)

The engines examined covered the following types:—

British: Merlin, Mercury, Hercules, Tiger.

French: Hispano, Gnome-Rhone.

U.S.A.: Cyclone, Twin-Wasp.

All the highly stressed parts (crankshaft, connecting rods, bearings) were carefully examined as to composition and heat and surface treatment. The survey also included cylinder liner, piston rings, valves, valve seating, springs, gears and cylinder bolts. A special section is reserved for light alloys (pistons, cylinder heads and crankcase). (The Cyclone is the only engine examined possessing a steel crankcase.)

Special attention is called to the French process of die casting cylinder heads, which is described in some detail. The author is of the opinion that British and French designers use needlessly complex alloy steels containing varying proportions of Cr, Ni, Wo, etc. Low alloy steels give equivalent performance, as is also recognised by America. Whilst nitriding appears to be more common than in German designs, the author considers that the surface finish is generally below the German standards.

Three New Aero Engines of the B.M.W. 132 Series. (Luftwissen, Vol. 8, No. 2, Feb., 1941, pp. 57-59.) (R.T.P. Translation No. 1,204.) (91/24 Germany.)

The three engines described are known as Mark F, K and N respectively and are further developments of the well known 132 series, 9-cylinder radial, bore=155.5 stroke=162.0 mm. The main improvements concern increased finning of the cylinder head round the exhaust valve port (the inlet valve port has no fins), the substitution of epicyclic reduction gears of the spur wheel type for the conical level gear and the fitting of fully automatic fuel injection pumps. Details of the general lay out of the engines and reduction gears are given. It

is stated that the cooling of the engine has also been improved by a new system of baffles attached to the outer ring cowling in such a way as to reduce flow losses to a minimum. No details of the cowling are given. Two valves per cylinder are fitted, inclined at 70°, the exhaust valve being sodium cooled. Both valves are fitted with a special spring clip to prevent the valve dropping into the cylinder in case of spring failure.

The auxiliary drives for injection pump, magneto, generator, air compressor, rev. counter and airscrew governor are neatly arranged on a separate plate at the rear of the engine.

Models F, K and N differ as regards supercharge layout and are rated as follows:—

	F	K	N
Maximum h.p. take-off ...	800	960	865
Continuous output ...	650	690	665
At altitude (M.) ...	4,300	1,800	4,500

Couplings and Clutches for Power Plant Machinery. (Engg. and B.H. Rev., May, 1941, pp. 352-358.) (91/25 Great Britain.)

This article gives particular prominence to the problems connected with the alignment of shafts in power plant drives, and formulæ are derived for correcting misalignment. The features and characteristics of a wide range of couplings for turbo-alternators and auxiliary drives of all kinds are dealt with to some length.

(Abstract supplied by Research Dept., Met. Vick.)

Air-cooled v. Liquid-cooled Aircraft. (J. G. Lee, J. Aeron. Sci., Vol. 8, No. 6, April, 1941, p. 219-229.) (91/27 U.S.A.)

Data are presented on the drag, weight, cooling and fuel consumption of air-cooled and liquid-cooled power plant installations. Based upon these data the design of three groups of air-cooled and liquid-cooled aeroplanes is postulated. When these groups are compared upon a basis of equal size and weight, the air-cooled aircraft are found to be superior in the pursuit, bomber and transport types. In the author's words: "The U.S.A. are in an extremely fortunate position to have in production 2,000 h.p. air-cooled engines—30 per cent. more powerful than anything available abroad. The foreign nations would match them if they could, but they are learning, as some Americans have already learned, that to develop a really satisfactory 2,000 h.p. liquid-cooled engine is truly a monumental task."

Possibilities of the Two-Stroke Cycle for Small Aircraft. (A. R. Rogowski, J. Aeron. Sci., Vol. 8, No. 6, April, 1941, pp. 230-235.) (91/28 U.S.A.)

In order to reduce the first cost and maintenance of the small aeroplane, and thus making private flying universally available, there is need for a simple, reliable, low-cost engine performance equal to the present four-stroke unsupercharged power plant. The piston-ported loop-scavenged two-stroke engine is considered for this purpose, using as a basis the results of tests on an experimental cylinder of this type. It is concluded that this engine would be most satisfactory, provided the fuel consumption at high outputs could be reduced by means of relatively inexpensive fuel-injection equipment.

The Dynamic Absorber and its Application to Multi-Throw Crankshafts. (Bailey and Bullied, J. Inst. Mech. Engrs., May, 1941, pp. 73-82.) (91/30 Great Britain.)

The dynamic absorber is stated to be the special case of a tuned absorber in which the natural frequency of oscillation is directly proportional to the rotational speed of the shaft which carries it. Four typical absorbers are studied in detail. In each case the tuning and amplitude equations are derived and, for

the roller types, expressions are obtained for the maximum roller amplitude which may be attained without the occurrence of slipping. It is stated that the method is quite general; and can be applied to any other type of engine as desired.

(Abstract supplied by Research Dept., Met. Vick.)

Method of Computing the Dimensions of Airplane Engine Coolers. (J. K. Thornton and J. G. Beerer, *J. Aeron. Sci.*, Vol. 8, No. 7, May, 1941, pp. 292-299.) (91/31 U.S.A.)

A theoretical analysis of the aeroplane engine air-air intercooler has been developed. As a result of this study, three simultaneous equations are obtained, which are solvable for the three linear dimensions of the intercooler. Certain constants in these equations can be obtained only from experimental tests data of the particular type of cooler under consideration. However, once these constants have been obtained, then the size of intercooler required to satisfy a given set of operating conditions may be correctly predicted.

The operating conditions are determined by specifying the following values:— (1) Engine air weight flow, initial temperature and pressure, required temperature drop and allowable pressure drop; (2) cooling air weight flow, initial temperature and pressure and allowable pressure drop.

If all these conditions are fixed, then the dimensions and volume of a given type of intercooler satisfying them are uniquely determined.

But in a practical case, considerable latitude may often be taken in the value of the weight flow of cooling air, in which case many different intercoolers will satisfy the remaining operating conditions. As the weight flow increases, all three dimensions of the intercooler change, but in such a manner that the volume decreases, consequently the final choice must be a compromise between the space available for the intercooler, the weight of the intercooler and ducting problems.

Analysis of the experimental and structural data of a commercially available intercooler gave the necessary coefficients for this type of cooler. These coefficients were inserted in the theoretical equations and then, assuming operating conditions corresponding to the test data, the equations were solved for dimensions and volume. The volumes computed in this manner, checked within 6 per cent. of the volumes used in the test data.

Identification of Oils by Means of Interfacial Surface Tension Determinations (Oil/Water or Oil/Aqueous Solution). (F. Seclich, *Fette and Seifen*, Vol. 48, No. 1, Jan., 1941, pp. 15-20.) (91/32 Germany.)

All liquids are subject to internal pressure due to intermolecular attraction. As a result the liquid tends to occupy the smallest possible space and any attempt to increase the surface of the liquid is resisted by the force of surface tension. In the case of mixtures, the surface layer will consist predominantly of those molecules which have the least intermolecular attraction, the more "active" molecules being relegated to the interior. Thus the addition of oleic acid (characterised by polar molecules of high internal pressure) does not markedly change the surface tension of paraffin oil (low internal pressure). If, however, instead of determining the surface tension in air (as is usual) the interfacial surface tension of such mixtures against water or aqueous solutions is determined, a large reduction (especially for the first minute additions) is observed. The effect does not only depend on the nature of the "active" constituent present, but also on the time, temperature and exposure to light. The author suggests that investigations of this type not only throw light on questions of molecular constitution and stability of emulsions, but are also useful in checking constancy of oil supplied to specification, degree of refining, etc. For this purpose the author has designed an interfacial tensometer based on an instrument previously described by Lecomte du Norry (*J. Gen. Physiol.*, Vol. 7, 1925, p. 625). In this

instrument the force exerted by the interfacial layer on a platinum ring is measured by means of a torsion balance. The main difference between the author's and the original instrument consists in the fact that the critical force is now measured without breaking the film. It has been found that the breaking away of the ring from the film is never sudden but always preceded by a so-called "super-tension" phase, during which extension of the film is not accompanied by any further increase in the reading of the balance. By means of a simple optical device the approach of this stage is indicated and repeated readings can then be taken over long periods on the same film. (If the film breaks, the ring will traverse the oil and will have to be cleaned before reinsertion.)

Relationship of Viscosity to Rate of Shear. (L. J. Bradford and F. J. Villforth, Trans. A.S.M.E., Vol. 63, No. 4, pp. 359-362.) (91/33 U.S.A.)

This paper reports tests designed to check the validity of the assumption that lubricating oils belong to the class of a Newtonian fluid, which is defined as one in which the force required to shear it is directly proportional to the rate of shear. It is on this assumption, which in recent years has been questioned, that equations for the behaviour of bearings have been based. Experimental evidence is produced in support of Petroff's equation which states that the torque required to rotate a journal, concentric with its bearing, is directly proportional to the product of the absolute viscosity and the rate of shear of the fluid separating the journal and the bearing. The agreement of the results with those predicted by the Petroff equation upon the assumption of the independence of viscosity from the rate of shear holds for all of the oils investigated.

The Effect of Holes Provided with Screw Threads or Longitudinal Serrations on the Endurance and Fatigue Strength of Flat Light Alloy Strips. (H. Burnheim, L.F.F., Vol. 18, No. 2-3, 29/3/41, pp. 102-106.) (91/34 Germany.)

The alloy strips (6 mm. thick) were made of dural and electron respectively and were tested under pulsating load (0 to max.) at a frequency of 25 cycles per sec. Wohler curves of max. stress on a basis of total load cycles required for fracture were plotted over the range of 10^4 to 10^7 cycles. After 10^7 cycles, the curve becomes practically horizontal, *i.e.*, the fatigue limit is reached and the corresponding stress variations can be supported indefinitely. The higher stresses corresponding to smaller number of permissible load cycles are called "endurance" stress. Experiments were carried out with undrilled and drilled strips, the holes being either plain, threaded, or serrated. The effect of loading the holes by means of a transverse pin was also investigated. In addition to endurance and fatigue limits, the ratio of endurance of plain sample to drilled sample as well as the ratio ultimate tensile of sample to endurance was determined over a range of load cycles. The former ratio is defined as the notch sensitivity β_k , and is a maximum for both materials for the serrated holes. β_k for the threaded hole is greater than for the plain hole. The relative order of β_k is the same whether the holes are pin loaded or not, but the absolute values are considerably greater in the former case.

For dural β_k does not vary much with number of load cycles (*i.e.*, over the range endurance-fatigue) provided the holes are not pin loaded (average value 2). In the case of pin loading, β_k increases from about 2 to 4 over the load cycle range 10^4 to 10^7 .

For electron (unloaded holes) β_k varies from 2 to 3 over the same load cycle range, but from 2.5 to 9.5 in the case of pin loaded serrated holes.

Similarly, over the load cycle range 10^4 to 10^7 the ratio of ultimate tensile to endurance increases from about 3 to 21 from pin loaded serrated holes in the case of magnesium, but only from 3 to 14 for the corresponding case of duralumin.

It is therefore concluded that pin loaded points of electron are unsatisfactory if the holes are serrated. The following table gives the strength characteristics of the plain (undrilled) material.

	Dural.	Electron.
Ultimate tensile, kg./mm. ²	42.6	31.5
Yield point, kg./mm. ² (permanent extension 0.2 per cent.)	29.4	21.5
Extension, per cent. ($l/d=5$)	19.9	14.4
Fatigue strength, kg./mm. ²	15.0	14.0

A New Use for X-Rays in Industry. (Woods and Kenner, Electronics, April, 1941, pp. 29-31.) (91/36 Great Britain.)

Particulars are given of an industrial process which uses the ionisation of air caused by the presence of X-rays to pass a minute current which controls a pass-or-reject relay. This new process is automatic in operation and it is suggested that for inspection of large numbers of articles it will prove more efficient and practical than the normal visual fluorescent inspection methods. The apparatus described is stated to be readily capable of inspecting 1,400 table knives an hour.

(Abstract supplied by Research Dept. Met. Vick.)

Effect of Temperature on Coiled Steel Springs Under Various Loadings. (F. P. Zimmerli, Trans. A.S.M.E., Vol. 63, No. 4, May, 1941, pp. 363-368.) (91/37 U.S.A.)

In the author's opinion the experiments justify the following conclusions:—

1. The usual spring steels are reliable when stressed 80,000 psi or less up to temperatures of 350 F. Between 350 F and 400 F and, at stresses up to 120,000 psi, the same continuity of results is lacking, but with proper forethought some commercial success might be expected.
2. The use of ordinary spring steels over 400 F is not possible.
3. Steels, hardened and tempered after coiling into springs, at the same hardness value, have no advantage over springs made of pretempered wire properly blued, under the conditions investigated.
4. Stainless steel of the 18-8 type resists temperature and stress better than other spring steels, except perhaps high-speed steel.
5. A middle hardness range in quenched-and-drawn springs is preferable to either high or low ranges.
6. An optimum temperature to heat springs after coiling for heat resistance is the highest one which will not render the hardness or other physical properties of the material objectionable.
7. The present Swedish valve-spring wire stands heat very poorly, in fact, is less satisfactory than many other steels.
8. Both high manganese and silicomanganese steels equal the chrome-vanadium steel tested and may have commercial advantages.

Unit Method of Beam Analysis. (F. R. Shanley and F. P. Cozzone, J. Aeron. Sci., Vol. 8, No. 6, April, 1941, pp. 246-255.) (91/38 U.S.A.)

Various improvements in the methods of analysis for determining axial and shear stresses in box beams have been combined into a practical tabular method which permits a considerable saving of time. The method also eliminates some of the errors often made through injudicious use of the classical methods of analysis and offers a means of extending the process to include secondary effects, such as caused by "shear lag" and cutouts.

Fabric Bearings. (Procter, Mech. World, 30/5/41, pp. 369-370-380.) (91/39 Great Britain.)

The question of lubrication is considered, and it is stated that bearing pressures up to 6,000 lb. per sq. in. have been dealt with successfully by suitable lubrication with water and grease. For light loads graphitic impregnation without external lubrication may be employed. Mention is made of the application of fabric linings to footstep and collar thrust bearings.

(Abstract supplied by Research Dept. Met. Vick.)

X-Ray Analysis in Industry. (J. Sci. I., May, 1941, pp. 69-102.) (91/40 Great Britain.)

This issue contains the first part of a symposium on X-ray analysis in industry sponsored by the Institute of Physics. The industrial applications of X-ray analysis form the subject matter for the ten papers in this section, and included are such titles as—Some application of the X-ray powder methods in industrial laboratory problems, an X-ray examination of mechanical wear products and some examples of industrial testing of materials by X-ray diffraction. The second part of the symposium is planned to be published in the July issue.

(Abstract supplied by Research Dept. Met. Vick.)

Least Work Solution of Shear Lag Problems. (E. Reissner, J. Aeron. Sci., Vol. 8, No. 7, May, 1941, pp. 284-291.) (91/41 U.S.A.)

The problem of the distribution of stresses in the cover sheets of box-beams, acted upon by bending loads, is treated by assuming parabolic bending stress distributions across the sheets and by determining the spanwise variation of the shape of these paraboles with the help of the method of least work (Castigliano's principle). A second order differential is obtained for the spanwise variation of the vertex curvature of the stress parabolas (which in the ordinary beam theory are straight lines). The equation has constant coefficients if there is no taper in sheet width and thickness, variable coefficients for tapered sheets. The equation is found to be integrable in terms of elementary functions for untapered beams and for a rather general class of tapered beams. The solution for beams of constant cross-section is worked out explicitly and applied to the analysis of a series of beams having different load distributions. For beams of constant cross-section an approximate formula is developed for the amount of shear lag at the most highly stressed section, this being in general also the section of greatest shear lag. This formula depends on the ratio of sheet width and distance of the centre of gravity of the load curve from the root section, on the elastic moduli and on the relative stiffness of flanges and sheets. Further it is shown that a design is possible such that no shear lag occurs. The method developed, and extensions of it, should permit a relatively simple solution for most practical problems in this field of stress analysis.

Harvey Directional Control. (Inter. Avia., No. 753, 6/3/41, p. 6.) (91/42 U.S.A.)

A promising direction-finding instrument has been developed by the Harvey Machine Co., Los Angeles, Calif. The Harvey Directional Automatic Radio Control fully automatically flies an aeroplane along a straight-line course passing through two radio stations, the manufacturers guaranteeing an accuracy to within one degree at any point of the course, regardless of meteorological conditions. The range of the equipment is said to exceed 1,000 miles. The new Harvey instrument consists of a combination of two independent homing devices, the signals of which are opposed to each other. As long as the aircraft is on course, the difference between the two angles formed by the intersection of the plane's longitudinal axis with the line of the course will be zero, no matter how the machine may be headed to correct for wind drift. As soon as the aircraft departs from true course these angles are no longer equal and the signal of one

station will overbalance the other. By means of an amplification system these signals operate a servo motor actuating the directional rudder control; hunting along the course is avoided by making the amplification inversely proportional to the signal strength. The equipment weighs 60 lb.

Devices for Locating Airliners on Their Respective Courses. (Inter. Avia., No. 753, 6/3/41, p. 15.) (91/43 U.S.A.)

At about the same time two of the big American airlines, United Air Lines and Transcontinental and Western Air, announced new devices for the automatic supervision of the location of the airliners on their respective courses. The device of T.W.A. is very simple and consists for each schedule of a small aircraft model moving along an electrically operated worm at a speed regulated according to the pilot's flight plan. The main advantage of the invention is that the dispatching office is automatically warned by an alarm signal in case an aircraft passes over one of the check points along its course without making its radio report. Of much greater interest and representing much more than a technical plaything is the invention of United Air Lines. Without the aid of the pilot and even without his knowledge the location of every aircraft is determined by several ground stations taking bearings on the machine as soon as the crew gets into short-wave radio telephone communication with any ground station. The installation makes it possible to inform the ground personnel of any deviation from the true course and to warn the pilot accordingly.

Photo-Electric Humidity Measurement. (C. Strobel, E.T.Z., 6/6/40, pp. 515-518.) (91/44 Great Britain.)

The author describes a new photo-electric method of measuring the dew point, and permitting of exact measurement of the humidity in the air and other gases within the temperature range of -10 to $+25^{\circ}\text{C}$. He also gives an electric circuit which, without the use of vapour pressure or psychrometer charts, makes possible direct and linear indication of the relative humidity as a percentage on an electrical pointer instrument or recording apparatus.

(Abstract supplied by Research Dept. Met. Vick.)

Flight Level Indicator. (R. W. Knight, J. Aeron. Sci., Vol. 8, No. 6, April, 1941, pp. 242-245.) (91/45 U.S.A.)

1. Flight level indicators, uniformly measuring pressure altitudes above a non-adjustable base, provide a solution to the universal problem of maintaining cruising and holding altitudes.

2. Relating flight levels to compass directions assures maximum vertical distance between aeroplanes on intersecting courses.

3. Relating flight levels to compass directions provides a simple easy rule for pilots to follow.

4. The use of this instrument would permit great simplification of air traffic rules. Fewer and simpler rules mean less violation and greater safety.

5. The absence of any adjustments eliminates the possibility of incorrect settings.

6. Even though all pilots do not maintain the pointer in exact agreement with the magnetic compass, the danger of collisions will be substantially reduced.

7. While the flight level indicator may be used to check the altimeter it does not take the place of the altimeter. The function of the altimeter is the maintenance of terrain clearance, while that of the flight level indicator is the maintenance of interplane clearance.

8. The cost of such instruments built in volume would be relatively low.

9. The weight of 1.17 pounds and space occupied in the instrument panel are justified.

10. The flight level indicator may be used in connection with the autopilot as a means of automatically controlling cruising altitudes.

An Electro-Optic Pressure Indicator. (Robertson, Rev. Sci. Instr., March, 1941, pp. 142-148.) (91/46 Great Britain.)

The author describes improvements on a diaphragm type of engine pressure indicator. The indicator takes advantage of the fact that a polished metal diaphragm forming part of the combustion chamber wall will be deflected in the form of a spherical mirror when there is a pressure difference across it. The intensity of a beam reflected from this diaphragm will vary with the pressure and by measuring the changes in intensity of the beam an indication of the change of engine pressure is obtained. It is stated that the indicator may be used at any engine speed and that a special direct-current amplifier has been constructed for this purpose.

(Abstract supplied by Research Dept. Met. Vick.)

A Ballistic Meter for Measuring Time and Speed. (Reich, Toomim Rev. Sci. Instr., Feb., 1941, pp. 96-99.) (91/47 Great Britain.)

This paper describes a speedometer in which a ballistic galvanometer serves as the indicating and recording element. Current flow through the galvanometer is initiated and stopped by means of a thyatron controlled by two switches. It is stated that the instrument was designed primarily for the measurement of automobile speeds in traffic studies, and should have other applications.

(Abstract supplied by Research Dept. Met. Vick.)

Night Photography by Means of Mg. Flare. (Inter. Avia., No. 752, 27/2/41, p. 11.) (91/48 U.S.A.)

The possibility of taking perfect photographs at night by means of extremely powerful flares is described as a new, very effective weapon adopted by the U.S. Army Air Corps. The method has been developed by Major G. W. Goddard in co-operation with the Eastman Kodak Co. and consists mainly of heavy, cylindrical flares about 32 in. high and 7 in. in diameter which are dropped without parachute. Following its release the flare is fired automatically and the magnesium content burns up in an explosion, developing a flash of several million candlepower. The combustion is completed within one-sixth of a second, during which period an area of about 19 sq. miles can be sufficiently illuminated. The shutter of the camera is operated via a relay by a photo-electric cell activated by the explosion of the flare; the negative (8 by 10 in.) is exposed at the peak of the flash which is attained 1/5,000 of a second after the explosion. The period of illumination, which lasts only a fraction of a second, and the strong blinding effect of the flare is said to prevent the betrayal of the position of the reconnaissance aeroplane.

Influence of War Experiences on the Development of A.R.P. Lighting. (E. Kämmerer, E.T.Z., 13/6/40, pp. 537-541.) (91/49 Great Britain.)

The author discusses black-out measures for work-rooms under the following sub-headings: (a) mechanical black-out; (b) partially mechanical black-out in conjunction with technical lighting measures; (c) partially mechanical black-out in conjunction with brushing paints which are impervious to light; (d) suppression filter method as black-out (complimentary colours); (e) technical lighting measures; (f) luminous substances. In conclusion the question of external lighting is discussed.

(Abstract supplied by Research Dept. Met. Vick.)

A Study of the Development of Skill During Performance of a Factory Operation. (R. M. Barnes and J. S. Perkins, Trans. A.S.M.E., Vol. 63, No. 4, May, 1941, pp. 319-328.) (91/50 U.S.A.)

While in general the many studies into the nature of skill have been concerned with the total time required to accomplish a given task and the influence on time values of varying conditions pertaining to a specific operation, this paper

is primarily devoted to a time study of the elements entering into the performance of an industrial task. The investigation constitutes a pioneer effort to study the effect of practice on a typical factory operation, conducted under laboratory conditions.

The various aspects of the study on which information was sought are as follows:—

1. The effect of practice on a typical factory operation carried on under laboratory conditions.
2. The learning curves of the various elements of the operation as they were performed by each of the different subjects.
3. The consistency between subjects in learning the same element.
4. The effects of "speeding."
5. The dispersion and its relation to the average performance time.
6. The effects of fumbling on the normal learning curve.
7. The several ways in which a transport load and pre-position element was performed.
8. The effectiveness of several rating techniques on data of known quality.
9. The effect of practice on the relation of eye movements to hand motion.

Summing up the discussion the paper seems to prove the desirability of establishing time standards from data as compared with individual time studies; and indicates that jobs should be planned to avoid, as much as possible, conditions which might cause fumbles. Two-thirds of the improvement noted was in the elimination of fumbling and one-third was due to faster movements and better co-ordination.

On the Technique of Forecasting Low Ceiling and Fog. (J. J. George, *J. Aeron. Sci.*, Vol. 8, No. 6, April, 1941, pp. 236-241.) (91/51 U.S.A.)

As far as the formation of fog is concerned, air loses its maritime properties on being exposed to sunshine over land for only a few hours. Accordingly fog which forms over land may be called "radiation" when the trajectory of the air has been mostly continental, and "advection" when it has not been over land during the day preceding the formation of the fog. It is found that radiation fog forms only when the air has been under a cloud cover a part of the previous day, and a forecasting method for such formations is developed. The forecasting of advection fog is shown to be more complex, and various methods necessary in such work are discussed. Examples of each type are presented.

An analysis of the causes of errors being made at present in the forecasting of fog and low ceilings is made, and indicates that substantial improvement in short range forecasts of such conditions is possible at this time. Suggestions for the elimination of present faults are made and a systematic method of forecasting described.

Examples and Outline of Certain Modifications in Upper Air Analysis. (R. B. Montgomery and A. T. Spilhaus, *J. Aeron. Sci.*, Vol. 8, No. 7, May, 1941, pp. 276-283.) (91/53 U.S.A.)

The first part of this paper deals with methods of isentropic analysis based on the scaled values of data transmitted for the purpose by the United States Weather Bureau. The practical application of shear-stability ratio vectors is demonstrated. A logical order of analysis is presented, designed to make the fullest possible use of all data available. The preferred isopleths for direct representation are those of temperature, acceleration potential and specific humidity; a system of isopleth spacing convenient in conjunction with surface weather maps is employed.

In the second part the properties of various surfaces for upper air analysis are systematically studied. It is found that severe restrictions exist in the use of surfaces of constant entropy or potential temperature. All the properties dis-

cussed are, however, adequately satisfied by a surface of constant potential virtual temperature, a quantity newly introduced and defined as the potential temperature of matter of standard composition, in this case dry air, at the same pressure and density as the sample. The thermodynamic configuration of this surface is described by isotherms of virtual temperature.

Infra-Red Radiation. (Koller, G.E. Rev., March, 1941, pp. 167-173.) (91/52 Great Britain.)

This paper collects information on the production, transmission, reflection and measurement of infra-red radiation. The fundamental laws of radiation are outlined and detailed consideration is given to the various sources of infra-red and to the characteristics of the radiation when passing through different media. Mention is made of the several methods of detection and it is suggested that the high-vacuum thermopile and galvanometer is the most suitable for measuring infra-red radiation.

(Abstract supplied by Research Dept. Met. Vick.)

Pilot Balloons Made Out of Transparent Plastic Film. (K. Eisele, L.F.F., Vol. 18, No. 4, 22/4/41, pp. 147-154.) (91/54 Germany.)

It has been noted that pilot balloons made of rubber and designed for really high altitudes (~ 40 km.) seldom pass 30 km. without bursting. The author considers that the main reason for this difficulty is the deterioration of the rubber at the low temperatures existing at these altitudes. Replacing rubber by a very thin transparent plastic has not been successful, as these synthetic substances become very brittle at low temperatures. The difficulty can be overcome by spraying the foil with a dark cellulose varnish, provided the thickness of the deposit is suitable (if the deposit is too thin, insufficient radiation is absorbed; if too thick the inner layers of the film are shielded). The film material used by the author has a cellulose base and is known under the trade name of Cuprophan. The thickness is .0065 mm. and its weight 10 gm./m.². It is obvious that the construction of a balloon made of such thin, and moreover inelastic material, presents considerable difficulties. Some of these, as well as the method of launching finally adopted, are described. Preliminary tests with balloons of this type have proved promising. Several larger designs were in hand when the advent of the present war stopped further experiments.

The Resistance Coefficient of Commercial Types of Wire Grids. (B. Eckert and F. Pfluger, L.F.F., Vol. 18, No. 4, 22/4/41, pp. 142-146.) (91/55 Germany.)

The grids examined were made of round wire varying between 0.1 and 0.7 mm. diameter with number of meches/cm. ranging from 1.5 to 63. The grids were supported in a tube of 45 cm. diameter and the resistance coefficient C_w determined from the equation

$$C_w = \Delta p / (\rho/2) V^2$$

when Δp = pressure drop across grid.

V = air speed at entry to grid.

The results are expressed in the form of graphs giving C_w as a function of air speed, Reynolds number and solidity (at constant Re) respectively. Solidity is defined as (projected area of wire)/(area of grid boundary). Maximum air speed (m./sec.) and Re were of the order of 30 and 1,000 respectively.

Under the conditions of the test (flow at entry mainly laminar) C_w undergoes a marked diminution with increase in air speed between 2 and 100 m. per sec. At higher speeds C_w is practically constant.

From the data provided it is easy to construct wire grids having a given resistance coefficient for a certain grid boundary area. In conclusion, the authors attempt to obtain theoretical values of C_w and with the help of certain assumptions, agreement with experimental values can be obtained.

LIST OF SELECTED TRANSLATIONS.

No. 34.

NOTE.—Applications for the loan of copies of translations mentioned below should be addressed to the Secretary (R.T.P.3), Ministry of Aircraft Production, and not to the Royal Aeronautical Society. Copies will be loaned as far as availability of stocks permits. Suggestions concerning new translations will be considered in relation to general interest and facilities available.

Lists of selected translations have appeared in this publication since September, 1938.

MATERIALS.

TRANSLATION NUMBER AND AUTHOR.	TITLE AND REFERENCE.
1188 Kotzochke, P. ...	<i>Materials and Design Features of Captured (i.e., non-German) Aero Engines.</i> (Luftwissen, Vol. 8, No. 3, March, 1941, pp. 69-78.)
1189 Cornelius, H. ...	<i>Investigations of Some Steel Fittings in Captured Non-German Aircraft.</i> (Luftwissen, Vol. 8, No. 3, March, 1941, pp. 78-81.)
1196 Hollbach 6 ...	<i>Aircraft Materials.</i> (Deutscher Flugzeugbau (Handbook of the German Aircraft Industry), 1939, pp. 176-179.)
1200 Perkuhn ...	<i>Behaviour of Laminated Pressed Synthetic Resins Under Creep.</i> (L.F.F., Vol. 18, No. 1, 28/2/41, pp. 32-37.)

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1194 Hollbach 6 ...	<i>Meteorological Instruments.</i> (Deutscher Flugzeugbau) (Handbook of the German Aircraft Industry), 1939, pp. 117-122.)
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Notices and abstracts from the Scientific and Technical Press are prepared primarily for the information of Scientific and Technical Staffs. Particular attention is paid to the work carried out in foreign countries, on the assumption that the more accessible British work (for example, that published by the Aeronautical Research Committee) is already known to these Staffs.

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